



**Politecnico
di Bari**

Dipartimento di Meccanica
Matematica e Management

Giornata Studio “Giorgio Minelli”

LE PROSPETTIVE FUTURE DEI MOTORI A COMBUSTIONE INTERNA

Scuola di Ingegneria

Bologna, 20 Aprile 2018



Sulla propagazione della fiamma, le emissioni gassose e di particolato, il controllo e il monitoraggio della combustione

Alcuni studi teorici, numerici e sperimentali sui motori a combustione interna presso il Politecnico di Bari

Speaker

Elia Distaso

Referenti

Prof. Ing. R. Amirante

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Collaborano

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University of Wisconsin-Madison

Engine Research Center – Madison (WI)

Emer. Prof. Rolf D. Reitz



Consiglio Nazionale delle Ricerche

Istituto Motori - Napoli

Dott.ssa Bianca Maria Vaglieco



Agenda

Giornata Studio «Giorgio Minelli» sui Motori – Bologna, 20 Aprile 2018

1. Correlazioni analitiche per il calcolo della velocità di fiamma laminare

- Correlazioni per vari combustibili di interesse pratico

In Cantiere...

2. Soot formation and oxidation

- Investigazioni numerico/sperimentali sulla combustione ossigenata della benzina
- Ruolo dell'olio lubrificante
 - Campagne sperimentali

3. Idee sul monitoraggio e il controllo della combustione

- Miscele gassose real-time
- Misura a basso costo della pressione in camera



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1 Correlazioni analitiche per la fiamma laminare

- **Correlazioni per vari combustibili di interesse pratico**
 - Metano
 - Propano
 - Miscele binarie Metano/Etano Metano/Propano
 - Miscele ternarie Metano/Etano/Propano come surrogato per il Gas Naturale
 - Benzina

1 Correlazioni analitiche per la fiamma laminare

Formulazioni per combustibili puri

$$S_L (\phi, T_u, p_u) = S_{L0} \left(\frac{T_u}{T_0} \right)^\alpha \left(\frac{p_u}{p_0} \right)^\beta$$

$$T_0 = 298 \text{ K}$$

$$p_0 = 1 \text{ atm}$$

Gülder (1984) $S_{L0} (\phi) = Z W \phi^\eta e^{-\xi(\phi-\sigma)^2}$

Liao (2004)

$$\alpha (\phi) = a_2 \phi^2 - a_1 \phi + a_0$$

$$\beta (\phi) = -b_2 \phi^2 + b_1 \phi - b_0.$$

Fuel	Z	W [cm/s]	η	ξ	σ
CH ₄	1	38.85	-0.20	6.45	1.08
C ₃ H ₈	1	42.11	-0.25	5.24	1.10
Gasoline	1	36.82	-0.22	4.86	1.11

Fuel	a_2	a_1	a_0	b_2	b_1	b_0
CH ₄	4.9199	10.287	6.9258	1.3712	2.6808	1.7492
C ₃ H ₈	2.7620	5.8808	4.9221	0.9250	2.0000	1.3560
Natural Gas	5.7500	12.150	7.9800	0.9250	2.0000	1.3650
Gasoline	3.2800	7.5200	5.9300	0.9250	2.0120	1.3650

1 Correlazioni analitiche per la fiamma laminare

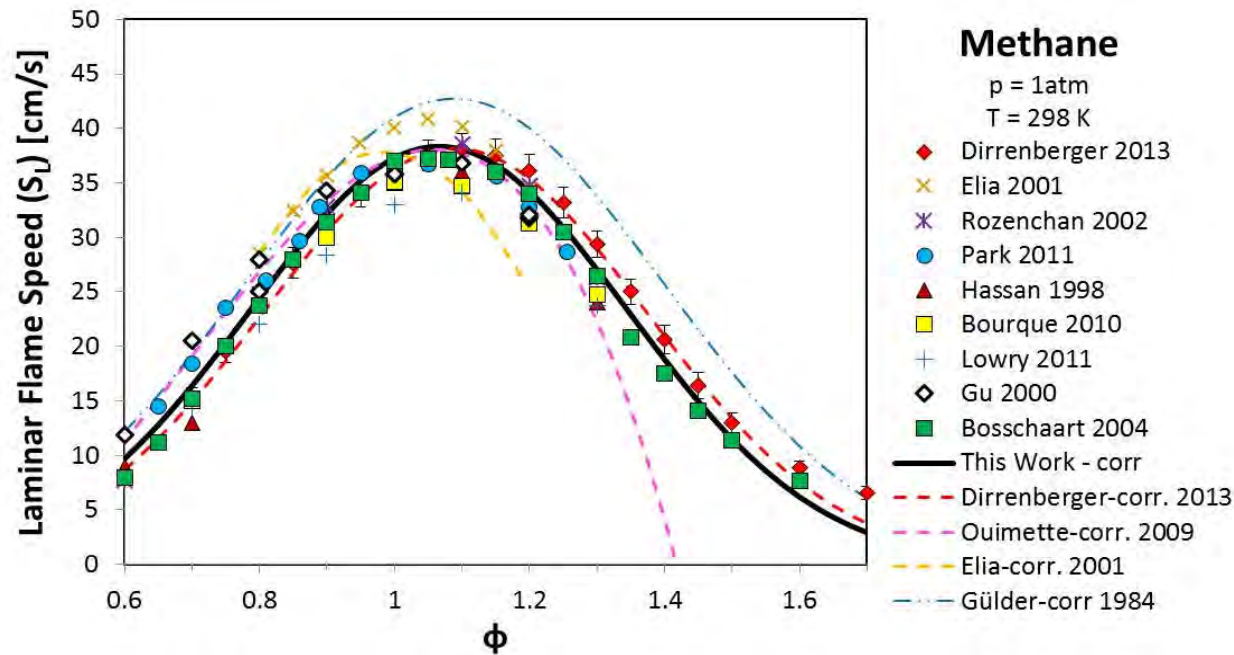
Risultati

$$p_0 = 1 \text{ atm}$$

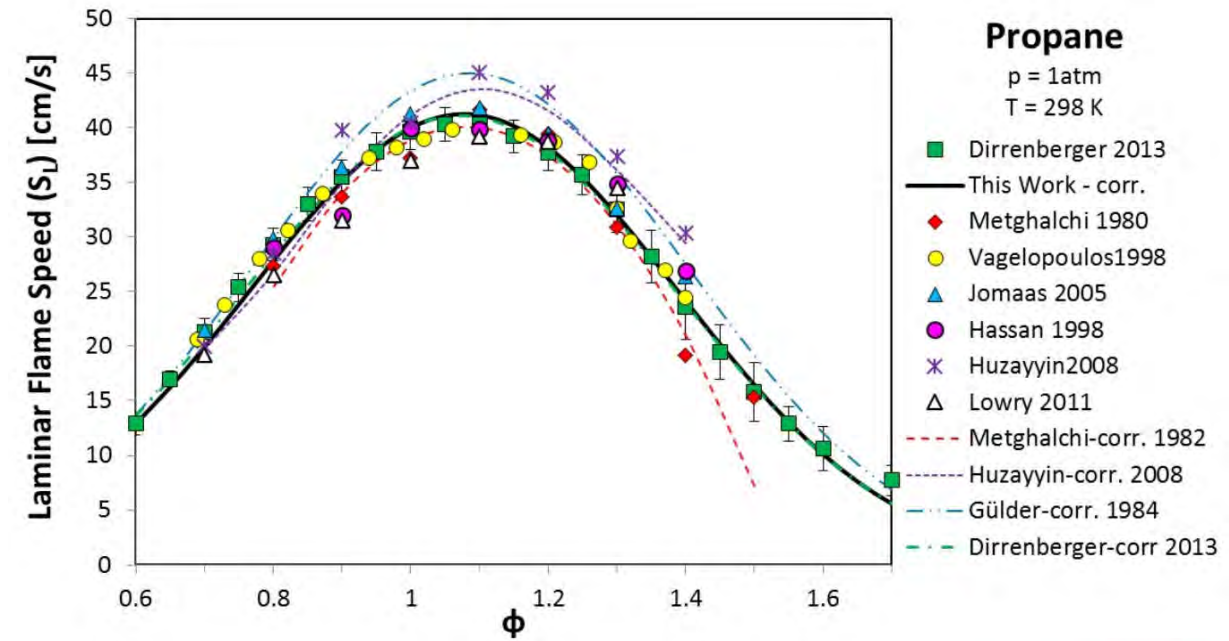
$$T_0 = 298 \text{ K}$$

$$S_{L0}(\phi) = Z W \phi^\eta e^{-\xi(\phi-\sigma)^2}$$

Methane



Propane



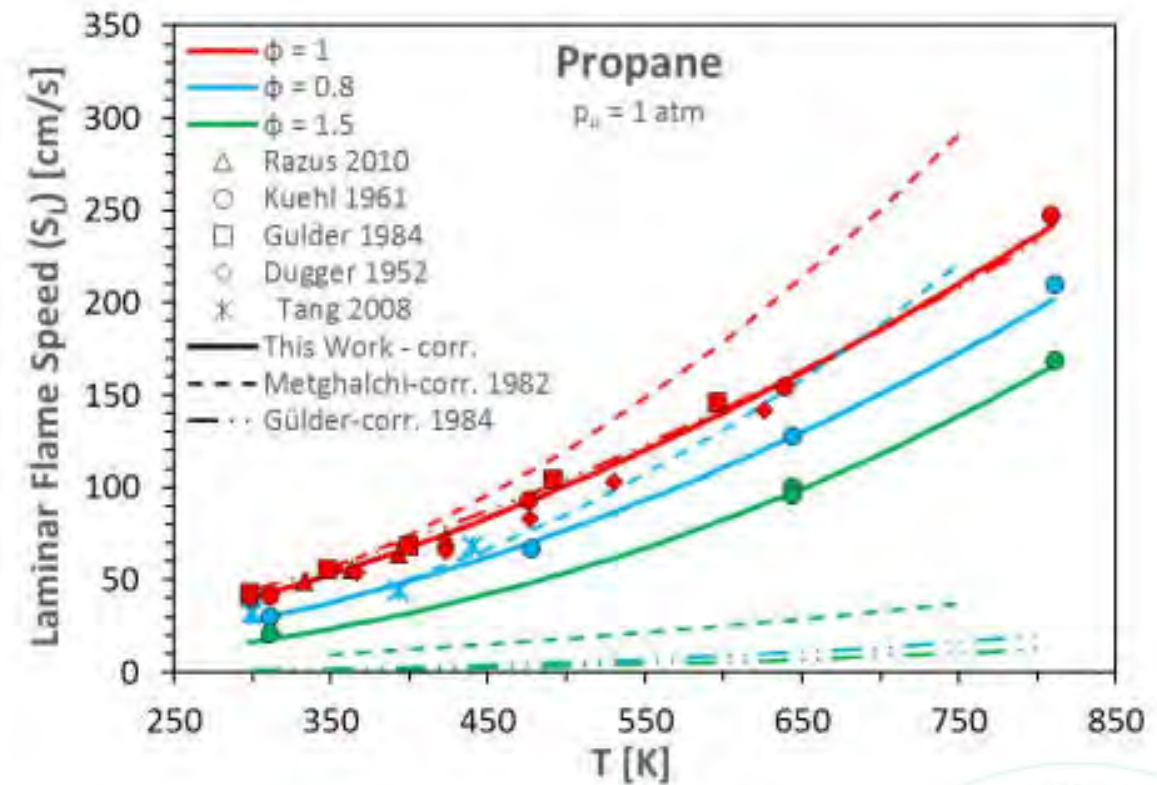
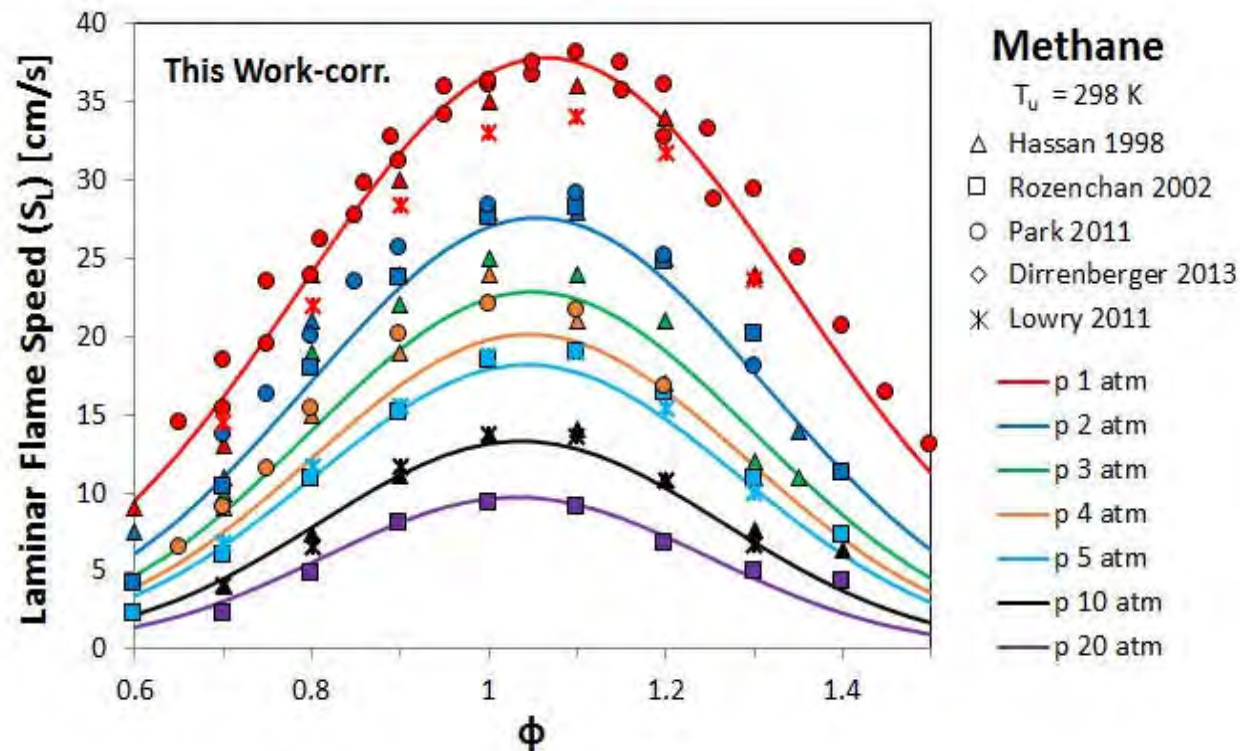
1 Correlazioni analitiche per la fiamma laminare

Risultati

P and T influence

$$\alpha(\phi) = a_2\phi^2 - a_1\phi + a_0$$

$$\beta(\phi) = -b_2\phi^2 + b_1\phi - b_0.$$



1 Correlazioni analitiche per la fiamma laminare

Formulazioni per miscele binarie e ternarie

Gülder (1984)

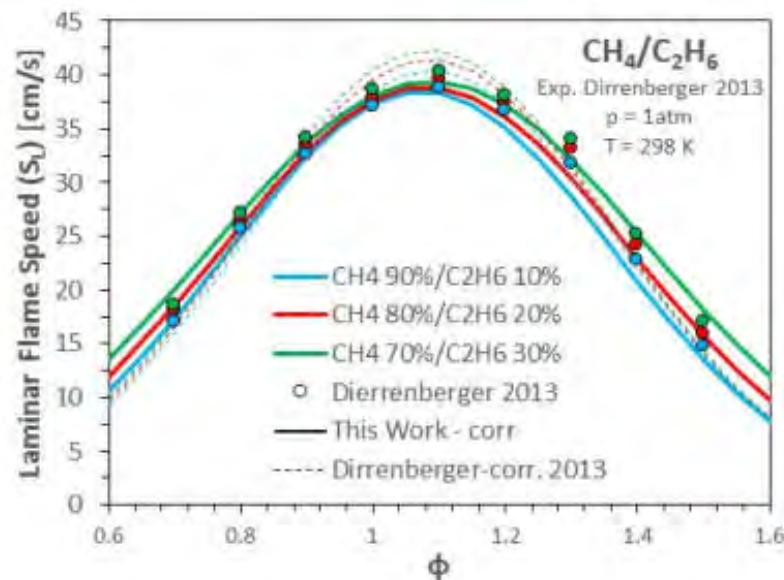
$$S_{L0}(\phi) = Z W \phi^\eta e^{-\xi(\phi-\sigma)^2}$$

Dirrenberger (2013)

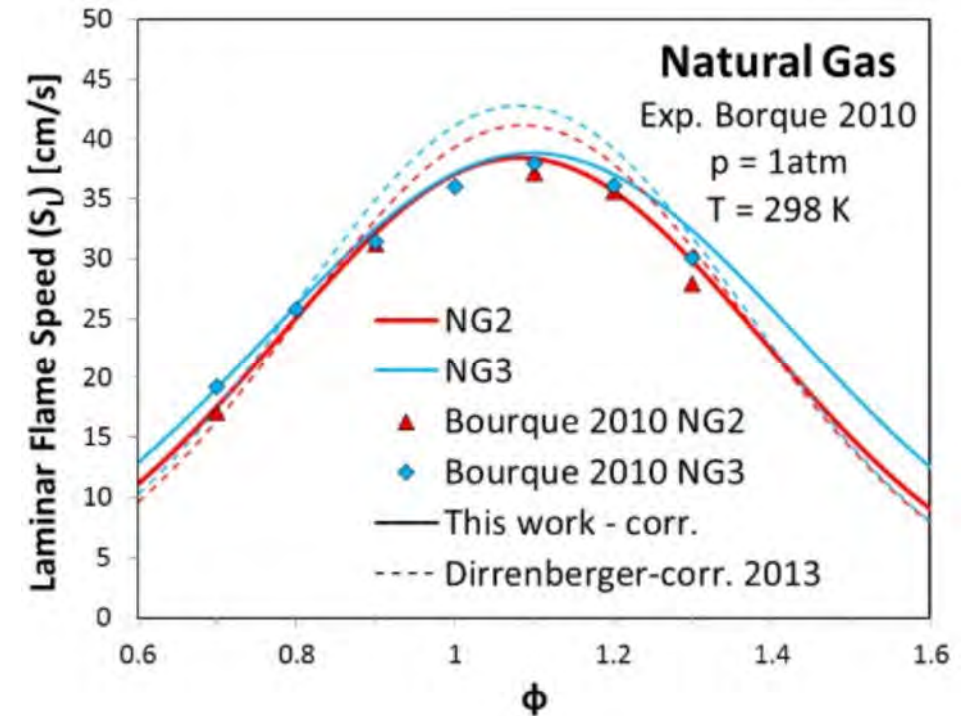
$$S_{L0}(\phi, \chi) = (1 + \nu \chi^\tau) W \phi^\eta e^{-\xi(\phi-\sigma-\Omega\chi)^2}$$

This work (2017)

$$S_{L0}(\phi, \chi) = (1 + \nu \chi^\tau) W \phi^{\eta(1-\chi)^\epsilon} e^{-\xi(\phi-\sigma-\Omega\chi)^2}$$



Miscele Binarie



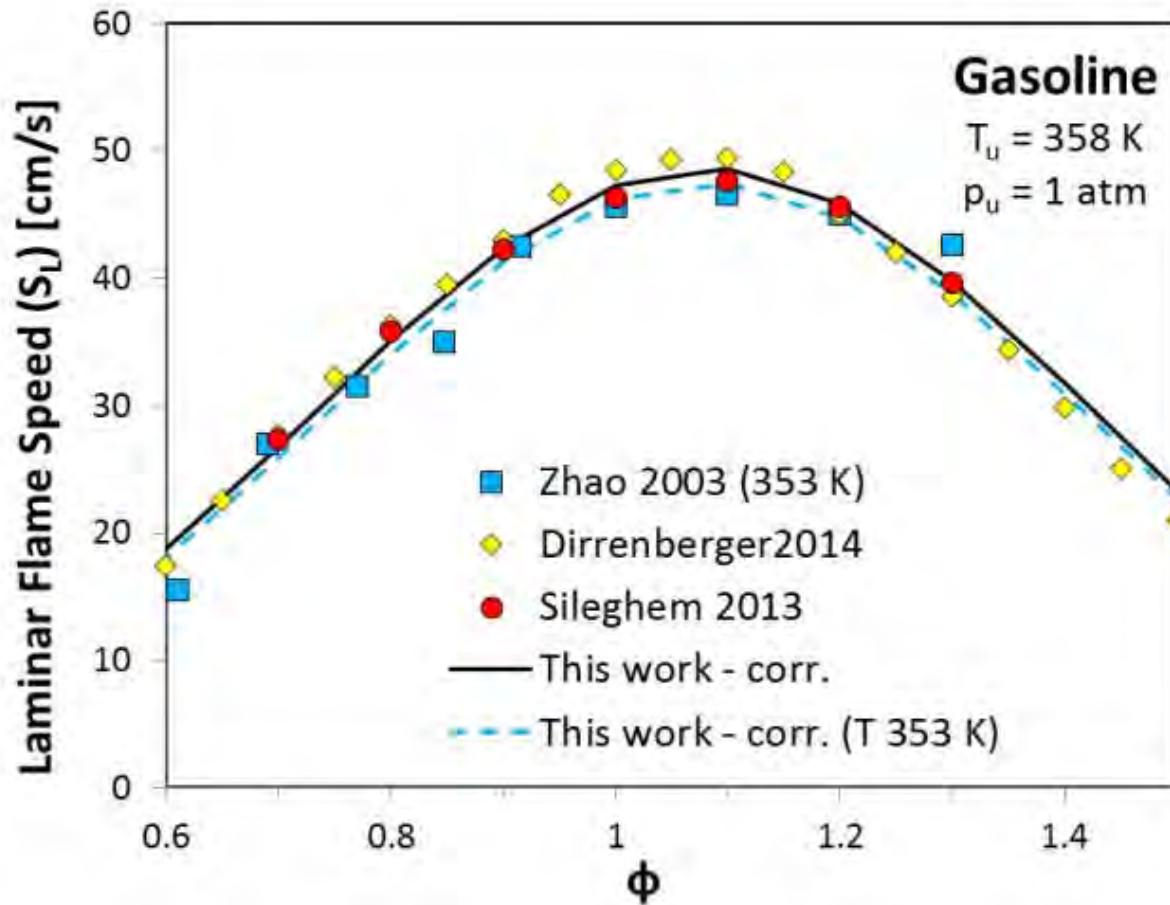
$$S_{L0}(\phi, \chi_1, \chi_2) = (1 + \nu \chi_1^{\tau_1}) (1 + \nu \chi_2^{\tau_2}) W \phi^{\eta(1-\chi_1)^{\epsilon_1}(1-\chi_2)^{\epsilon_2}} e^{-\xi(\phi-\sigma-\Omega_1\chi_1-\Omega_2\chi_2)^2}$$

Gas Naturale

1 Correlazioni analitiche per la fiamma laminare

Risultati

Gasoline

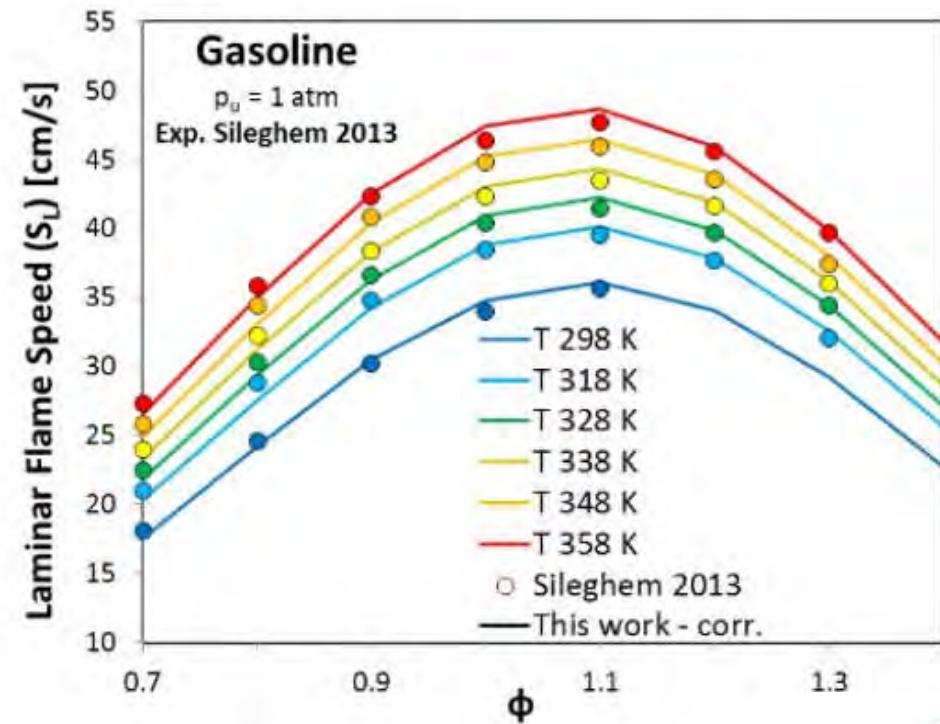


$$S_L(\phi, T_u, p_u) = S_{L0} \left(\frac{T_u}{T_0} \right)^\alpha \left(\frac{p_u}{p_0} \right)^\beta$$

$$S_{L0}(\phi) = Z W \phi^\eta e^{-\xi(\phi-\sigma)^2}$$

$$\alpha(\phi) = a_2 \phi^2 - a_1 \phi + a_0$$

$$\beta(\phi) = -b_2 \phi^2 + b_1 \phi - b_0$$



1 Correlazioni analitiche per la fiamma laminare

Amirante, R., Distaso, E., Tamburrano, P., & Reitz, R. D. (2017). **Laminar flame speed correlations for methane, ethane, propane and their mixtures, and natural gas and gasoline for spark-ignition engine simulations.** *Int. Journal of Engine Research*, 18(9), 951-970. doi:10.1177/1468087417720018

In cantiere...

- Allargamento ed aggiornamento del database di dati sperimentali di letteratura
- Idrocarburi **oltre i C_3**
- Combustibili **ossigenati** (Metanolo, etanolo,)
- Influenza di **inerti** (EGR, N_2 ,)
- Influenza di presenza di **acqua**
- Altre **miscele binarie** (metano/idrogeno, H_2/CO , propano/butano, ...)
- Miscele a più di 3 componenti
- Correlazioni per il **Syngas**
- Benzina come miscela e non combustibile puro



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2 Soot formation and oxidation

- **Investigazioni numerico/sperimentali sulla combustione ossigenata della benzina**
- **Ruolo dell'olio lubrificante**
 - Campagne sperimentali



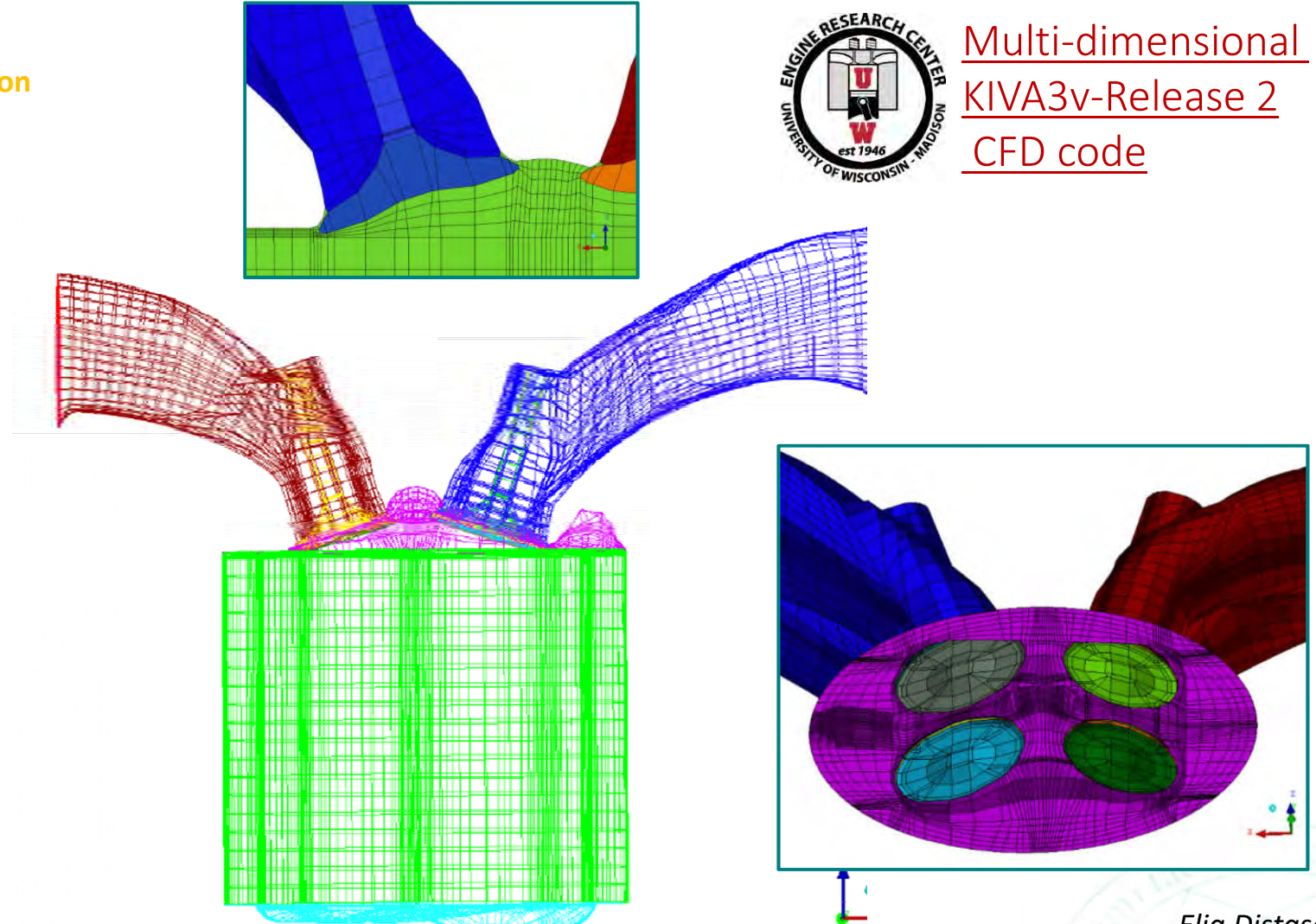
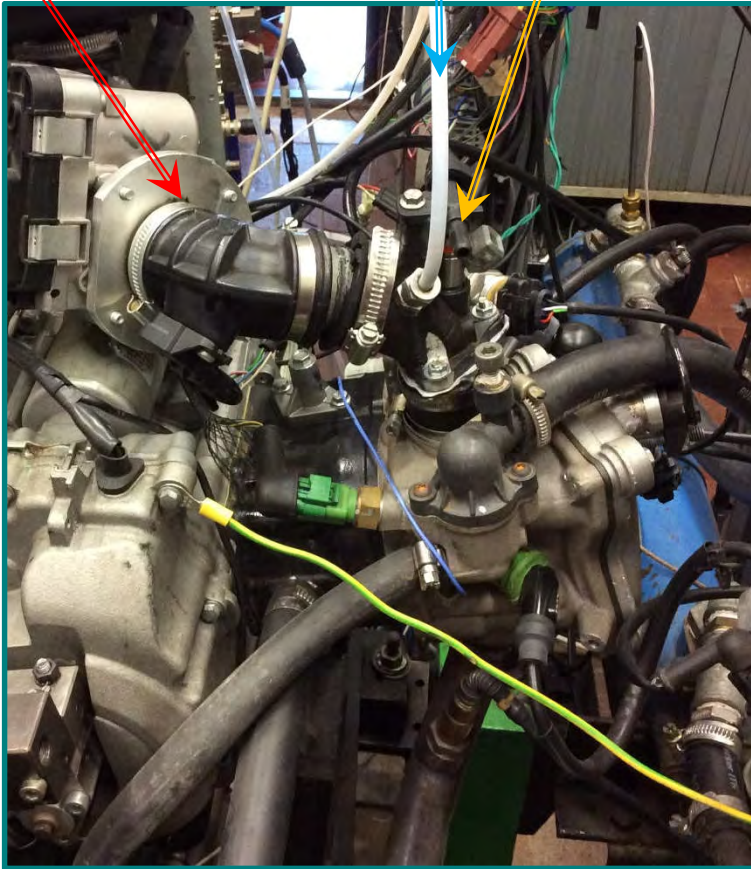
Elia Distaso

Politecnico di Bari

2 Combustione ossigenata della benzina

Soot Formation and Oxidation

Air inlet O_2 inlet Gasoline Port Injection



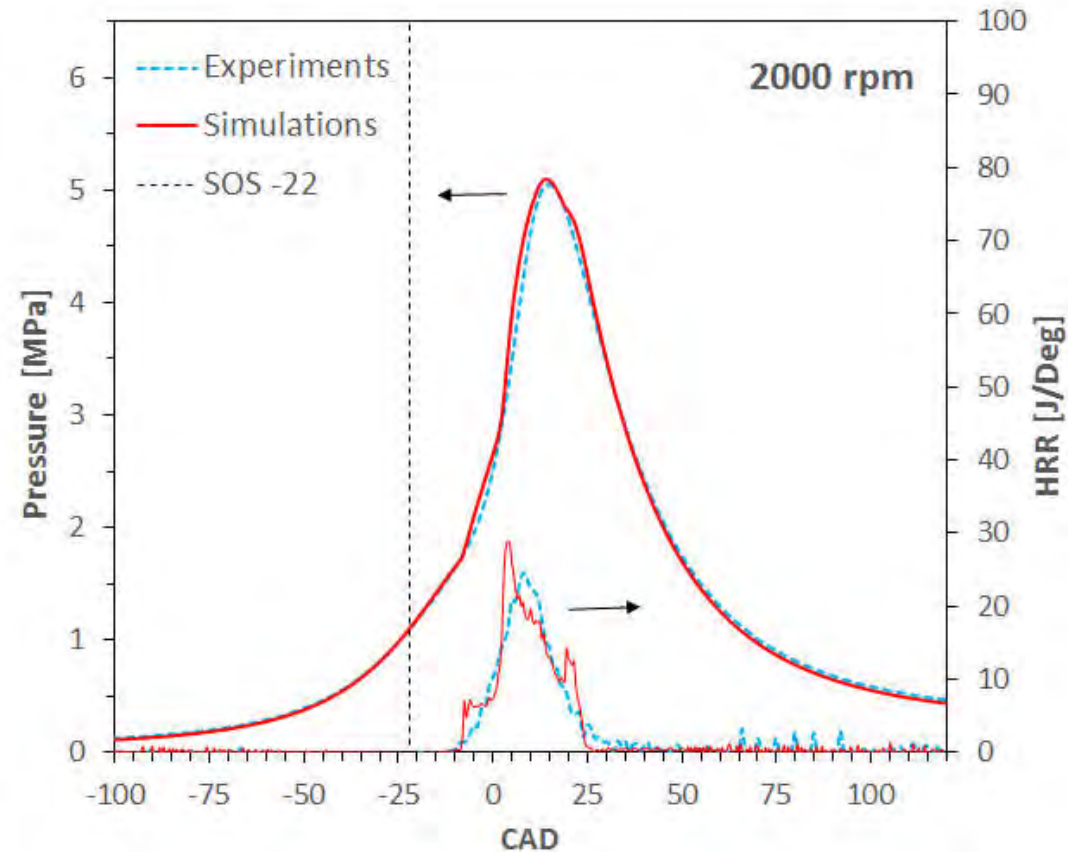
Multi-dimensional
KIVA3v-Release 2
CFD code

2 Combustione ossigenata della benzina

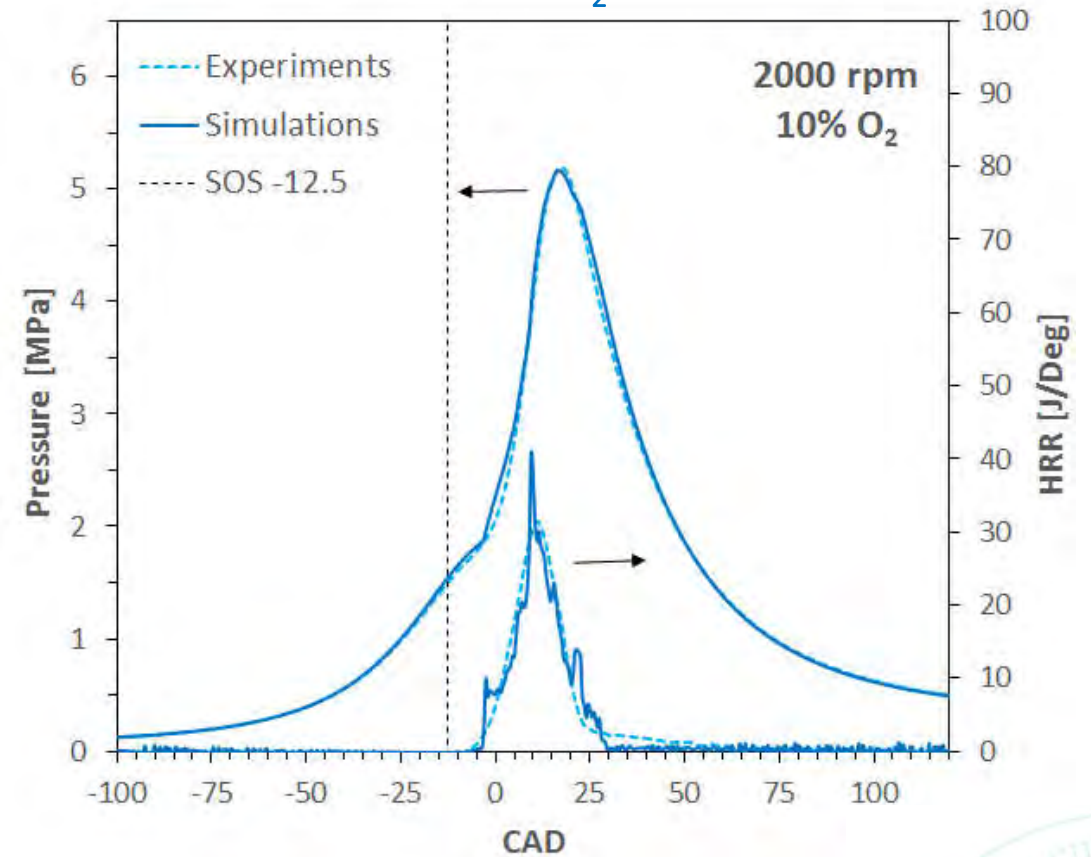
Soot Formation and Oxidation

2000 rpm

BASELINE



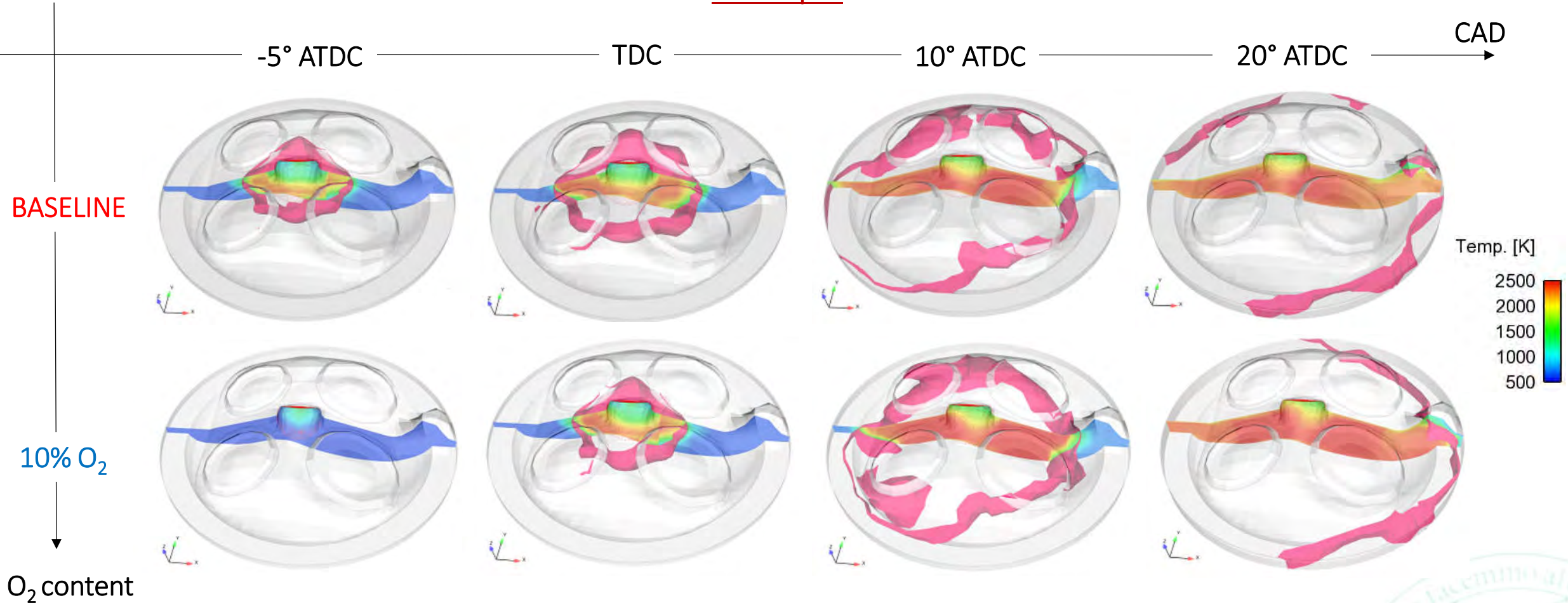
10% O₂



2 Combustione ossigenata della benzina

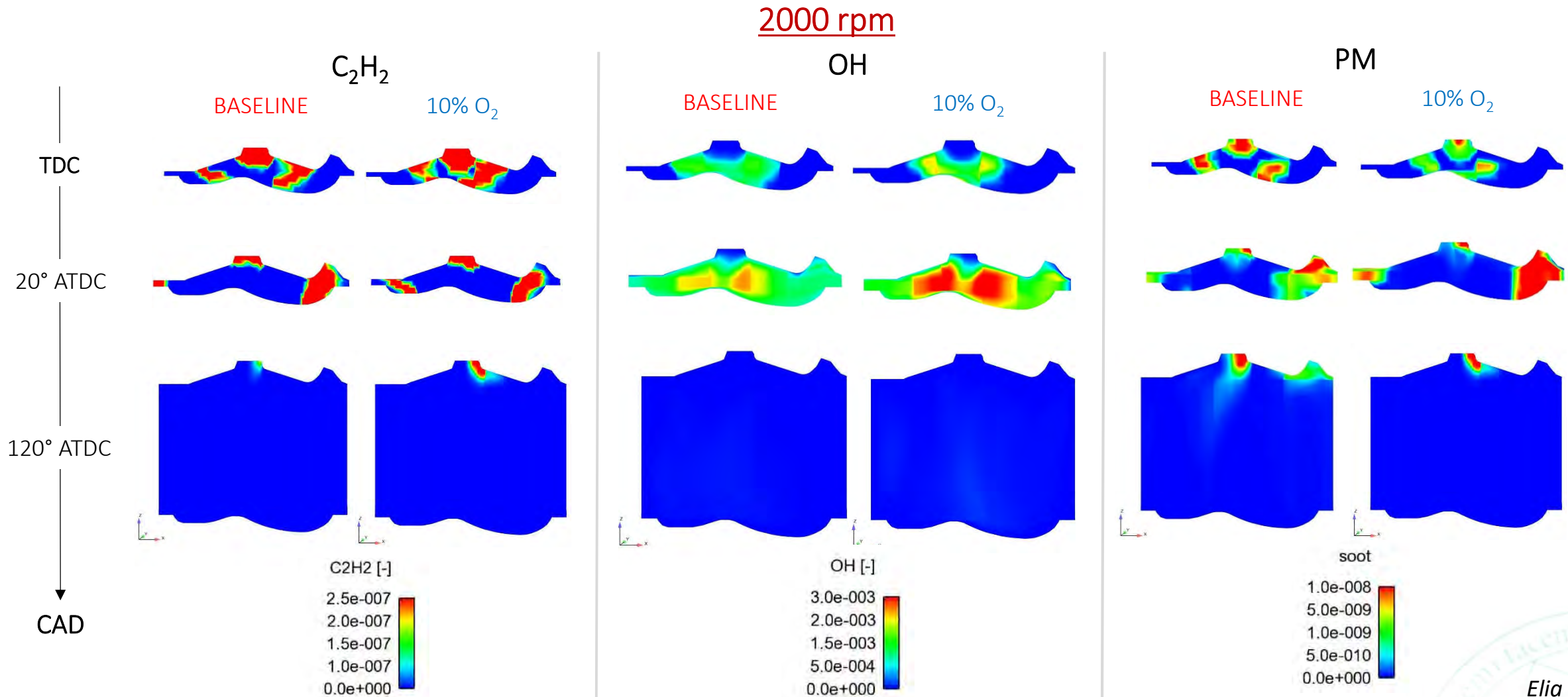
Soot Formation and Oxidation

2000 rpm



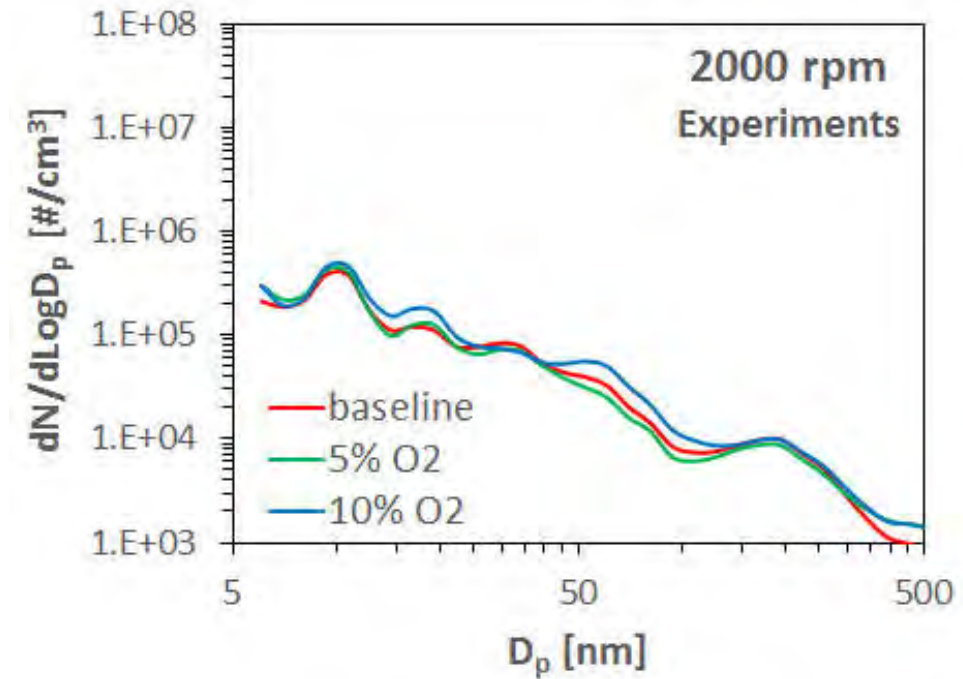
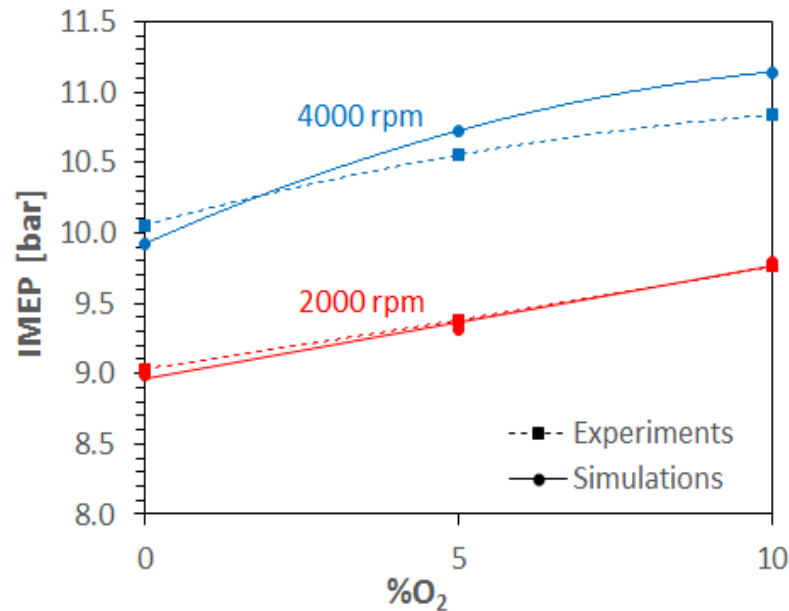
2 Combustione ossigenata della benzina

Soot Formation and Oxidation



2 Combustione ossigenata della benzina

Soot Formation and Oxidation



Amirante R, Distaso E, Tamburrano P., Reitz R.D.

Numerical Investigation of Load Effects on Particulate Emissions in Gasoline Spark-Ignition Engines.

Symposium for Combustion Control 2017; June 28th-29th, 2017, Aachen, Germany

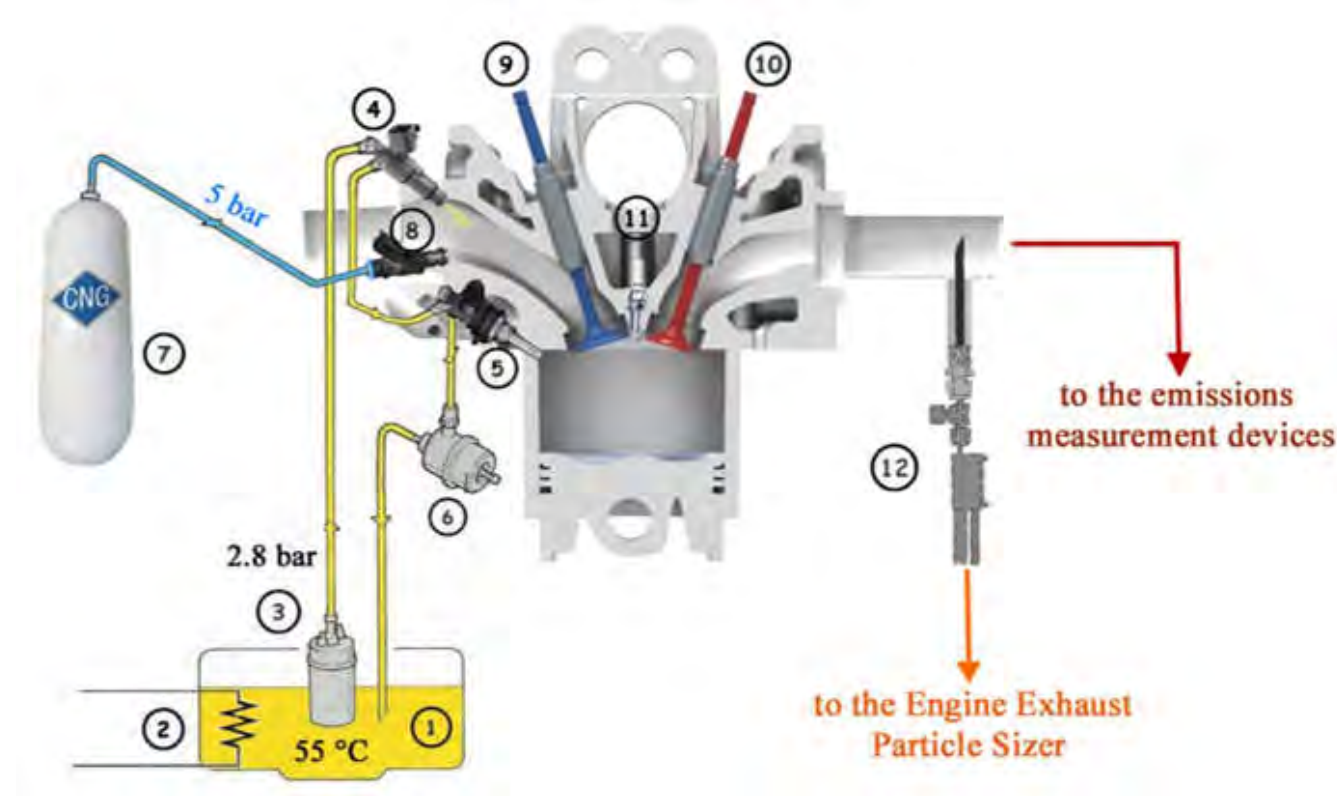
2 Ruolo dell'olio lubrificante

Campagne sperimentali

- “Oil-free” optical engine at 2000 rpm and full load
- Multi-grade, low viscosity, full-synthetic lubricant 0W-30
- Oil-to-fuel mass = 1, 3, 5, 7%

Optical engine specifications

Name	Units	Value
Cylinder volume	cm ³	250
Bore	mm	72
Stroke	mm	60
Compression ratio	None	10.5
Max power	kW	7.9 at 5000 rpm
Max torque	Nm	14.7 at 5500 rpm



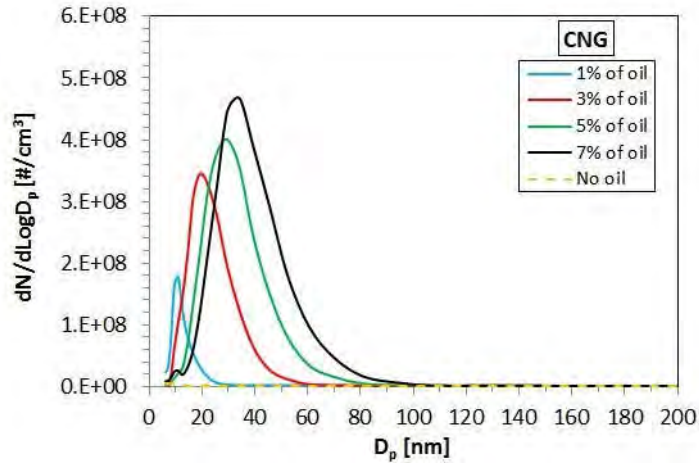
	PFI tests	DI tests
CNG tests	CNG → injector 8 oil → injector 4	CNG → injector 8 oil → injector 5
Gasoline tests	Gasoline + oil → injector 4	Gasoline + oil → injector 5

2 Ruolo dell'olio lubrificante

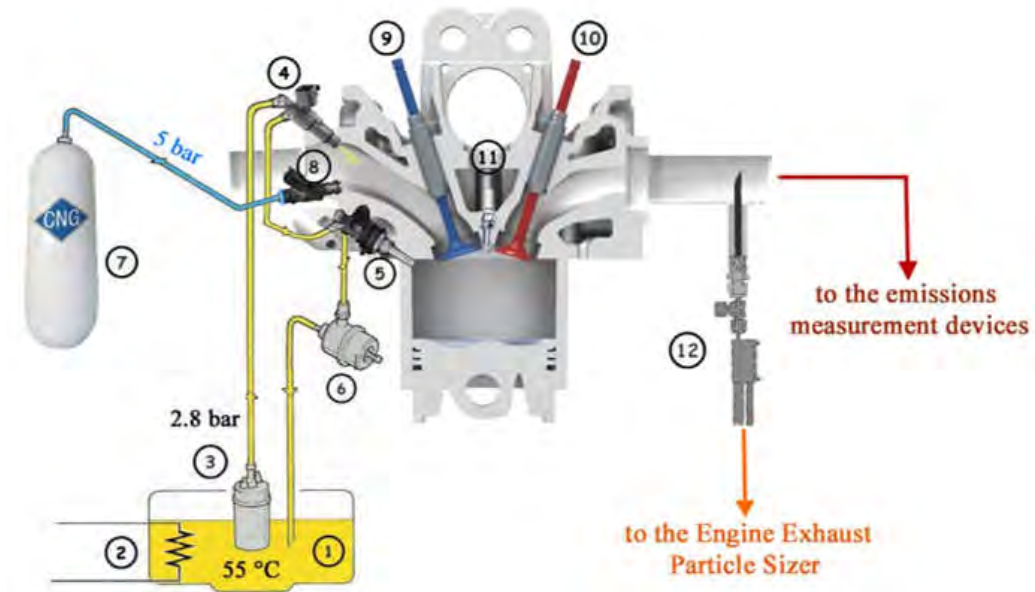
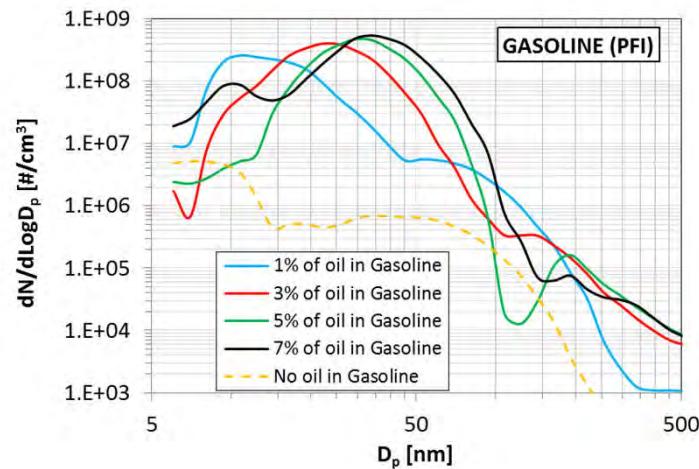
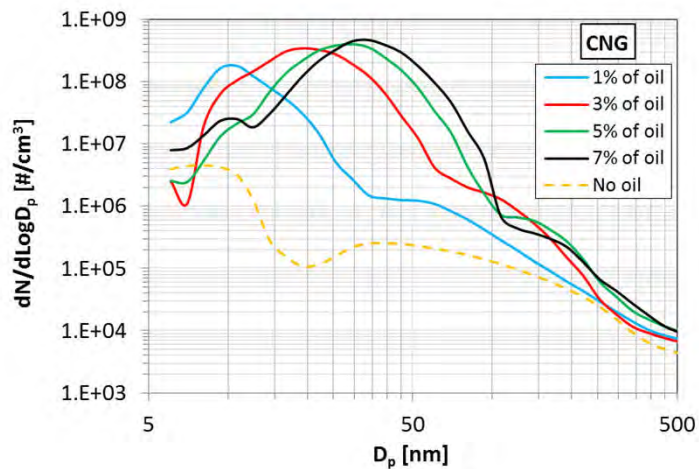
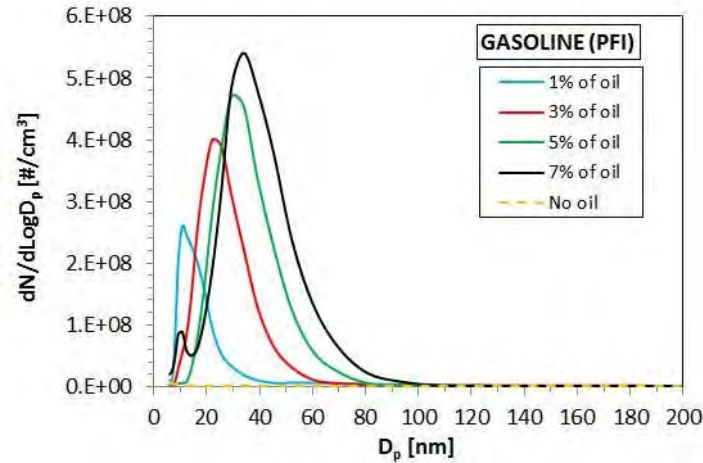
Campagne sperimentali

Campagne sperimentali

CNG



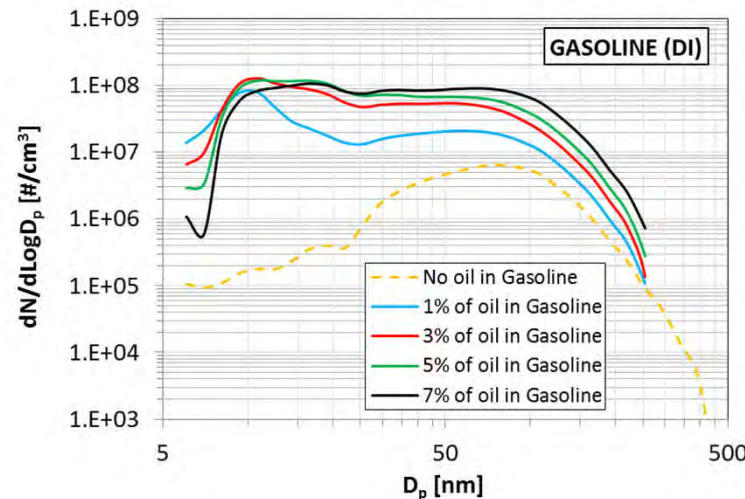
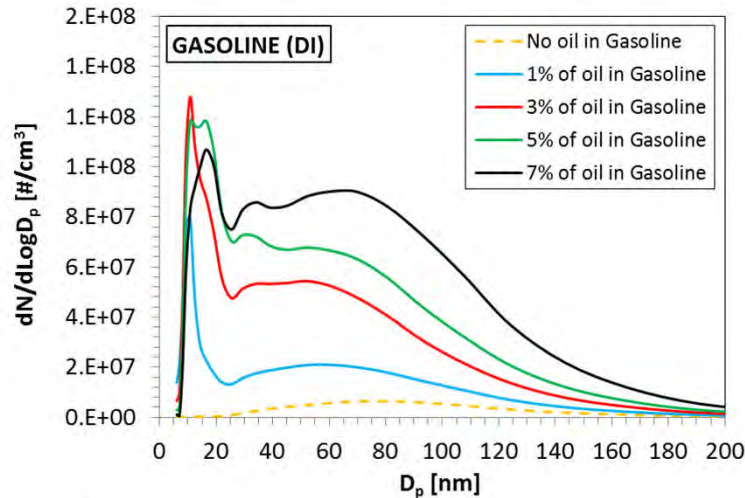
Gasoline (PFI)



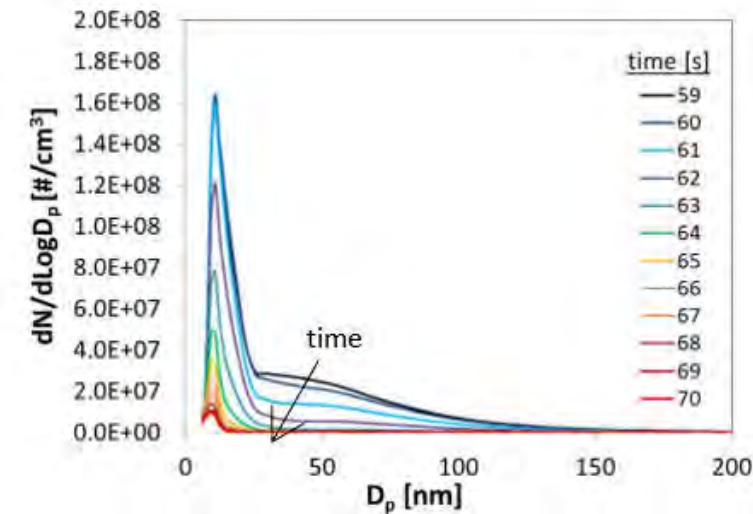
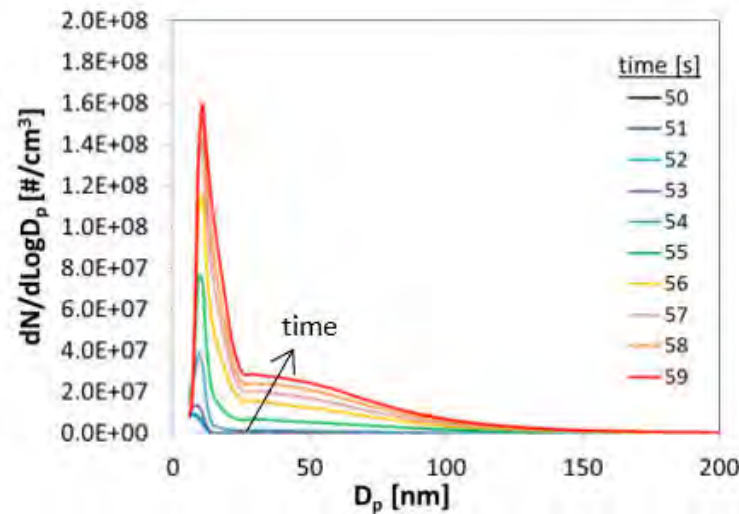
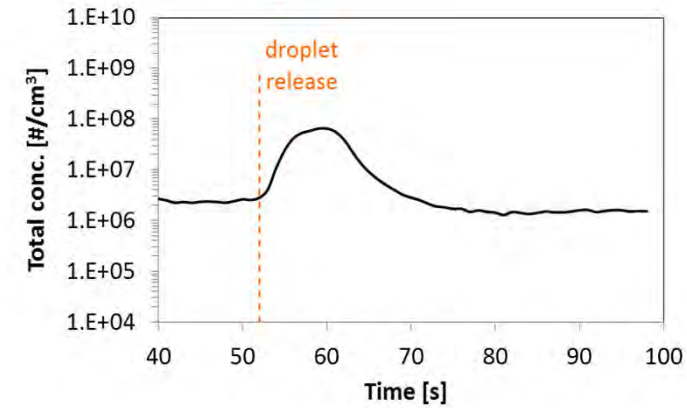
2 Ruolo dell'olio lubrificante

Campagne sperimentali

Gasoline (DI)



Emulation of oil droplet release with CNG-PFI



Amirante R, Distaso E, Di Iorio S, Napolitano M, Sementa P, Tamburrano P, Vaglieco B.M., Reitz R.D. Effects of Lubricant Oil on Particulate Emissions from Port Fuel and Direct Injection Spark-Ignition Engines. Int J Engine Res 2017;18:606-6202. doi:10.1177/1468087417706602



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3 Idee sul monitoraggio e il controllo della combustione

- **Miscela gassose real-time**
- **Misura a basso costo della pressione in camera**

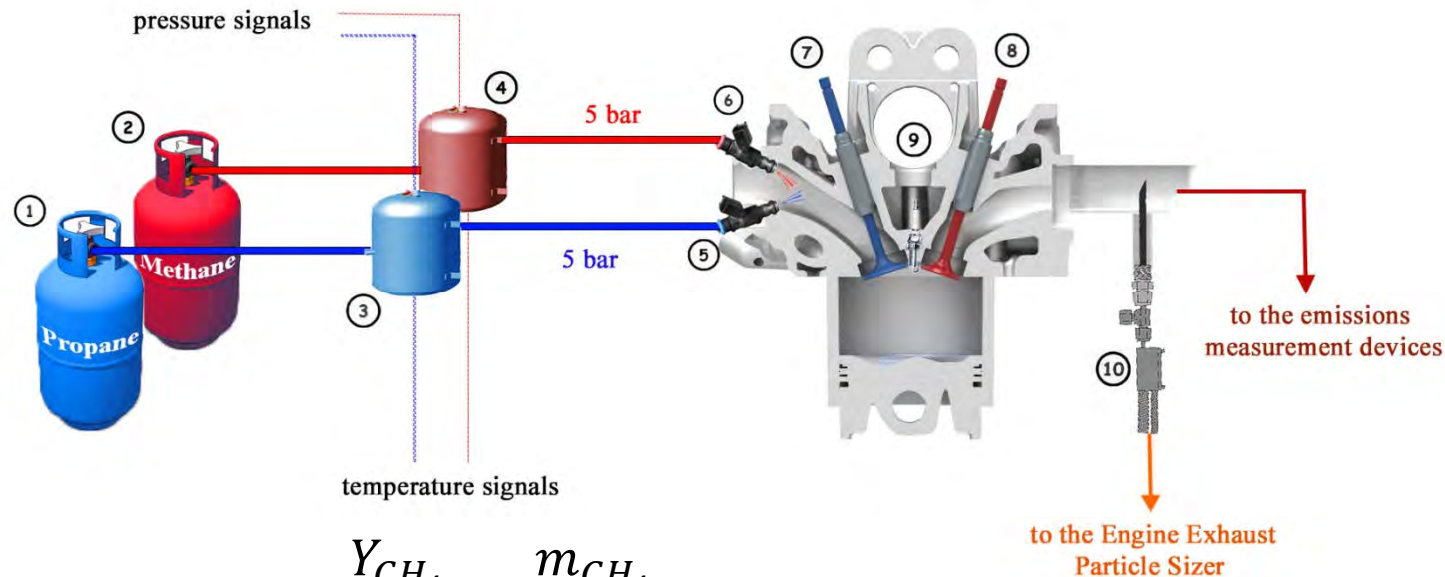


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Politecnico di Bari

3 Miscele gassose real-time

Idee sul monitoraggio e il controllo della combustione



$$\chi_{CH_4}, \chi_{C_3H_8} \rightarrow \frac{Y_{CH_4}}{Y_{C_3H_8}} \equiv \frac{m_{CH_4}}{m_{C_3H_8}}$$

$$\frac{\Delta t_{CH_4}}{\Delta t_{C_3H_8}} = C \frac{\chi_{CH_4}}{\chi_{C_3H_8}} \frac{p_{C_3H_8}^0}{p_{CH_4}^0} \sqrt{\frac{T_{CH_4}^0}{T_{C_3H_8}^0}}$$

$$\dot{m}_i = A_{inj} \frac{p_i^0}{\sqrt{R_i T_i^0}} \sqrt{\gamma_i} \sqrt{\left(\frac{2}{\gamma_i + 1}\right)^{\frac{\gamma_i + 1}{\gamma_i - 1}}}$$

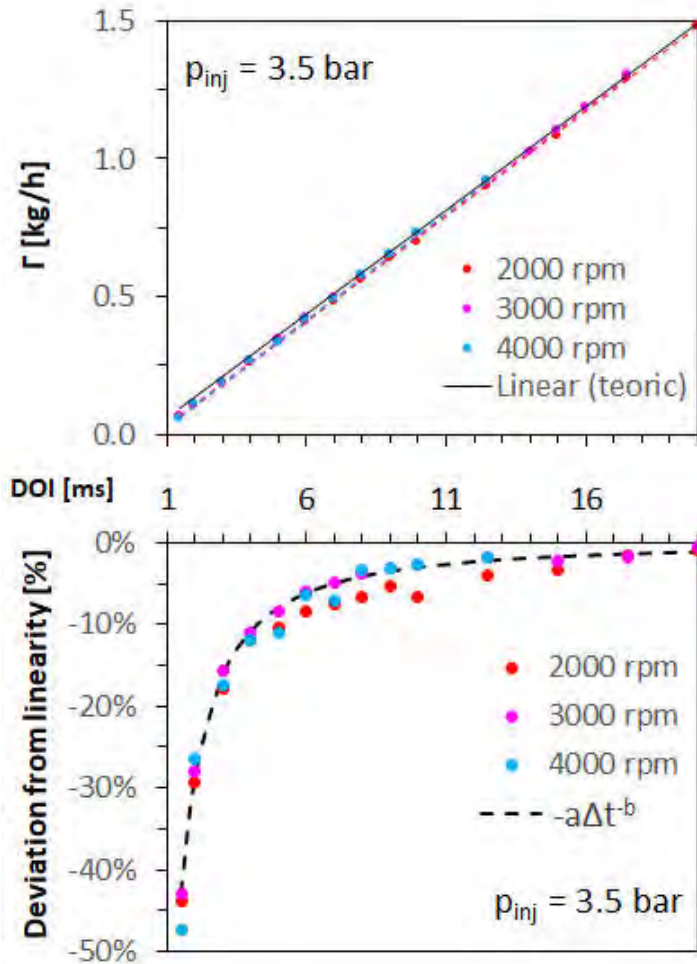
$$C = \frac{MW_{CH_4}}{MW_{C_3H_8}} \sqrt{\frac{\frac{\gamma_{C_3H_8}}{R_{C_3H_8}} \left(\frac{2}{\gamma_{C_3H_8} + 1}\right)^{\frac{\gamma_{C_3H_8} + 1}{\gamma_{C_3H_8} - 1}}}{\frac{\gamma_{CH_4}}{R_{CH_4}} \left(\frac{2}{\gamma_{CH_4} + 1}\right)^{\frac{\gamma_{CH_4} + 1}{\gamma_{CH_4} - 1}}}}$$

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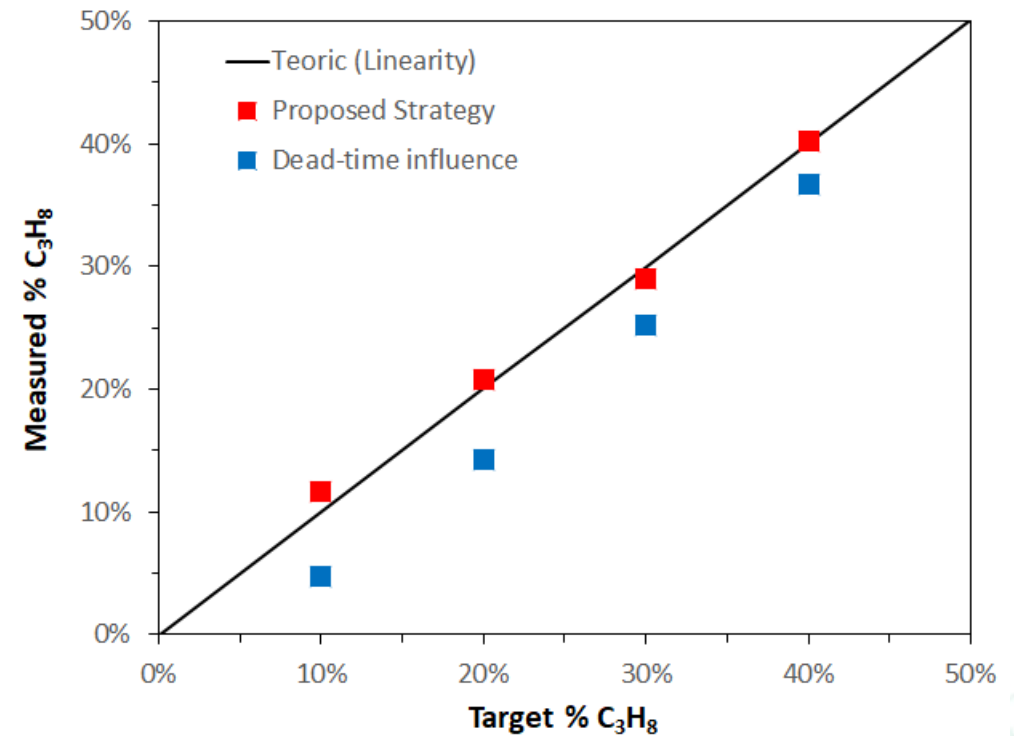
3 Miscele gassose real-time

Idee sul monitoraggio e il controllo della combustione



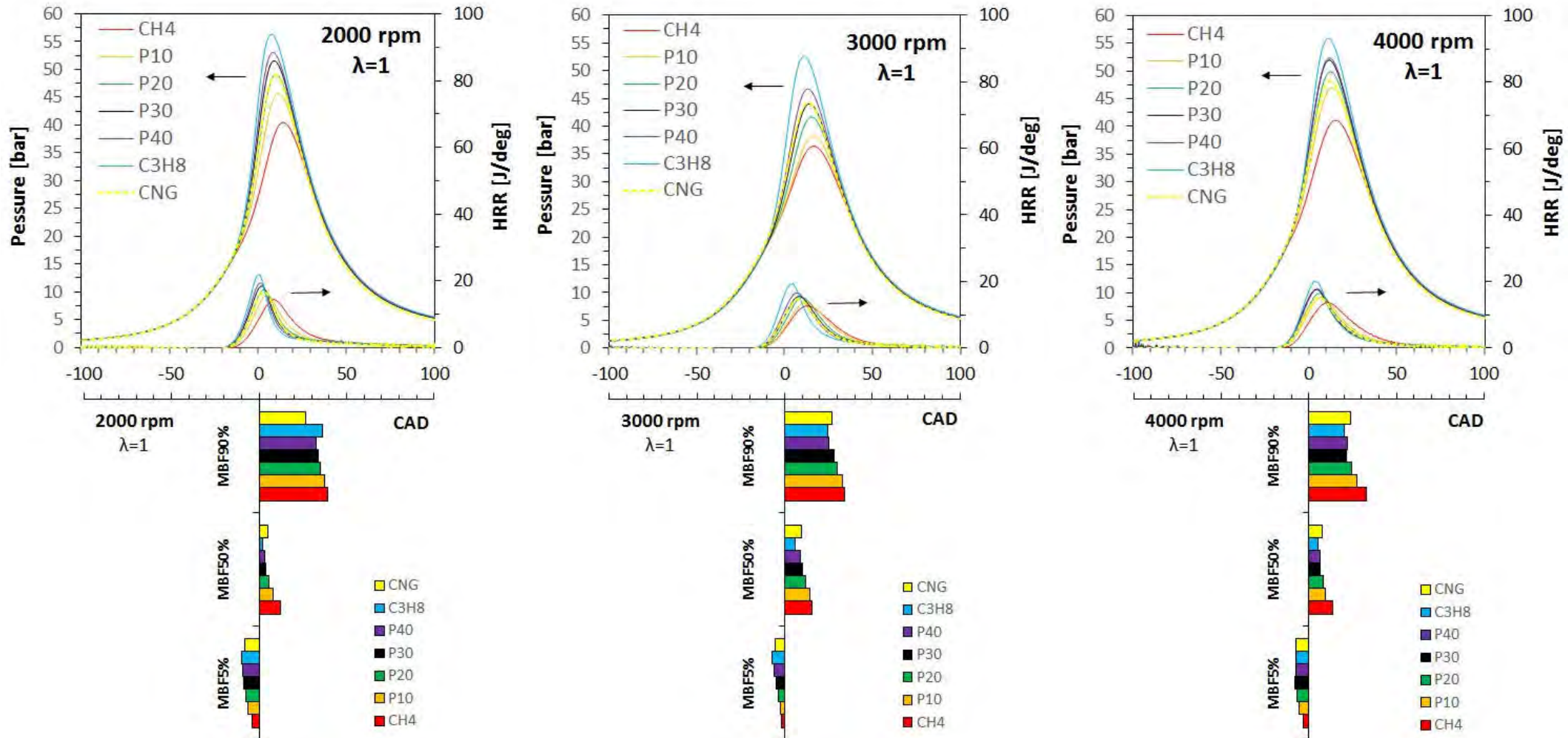
$$\dot{m}_i = A_{inj} \frac{p_i^0}{\sqrt{R_i T_i^0}} \sqrt{\gamma_i} \sqrt{\left(\frac{2}{\gamma_i + 1} \right)^{\frac{\gamma_i + 1}{\gamma_i - 1}} \frac{f_{inj}}{f_{inj}^{ref}} \left(1 - a \Delta t_i^{-b} \right)}$$

$$\Gamma = \frac{f_{inj}^{ref}}{f_{inj}} \dot{m}_{meas}$$



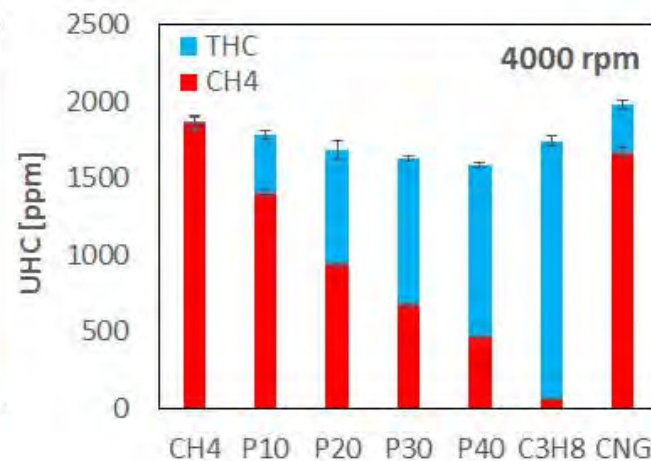
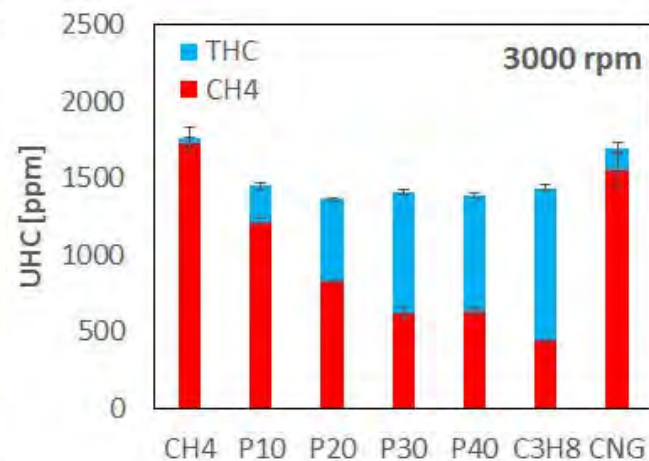
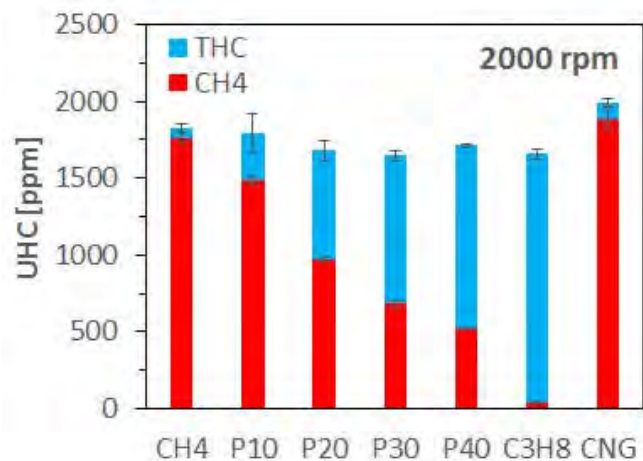
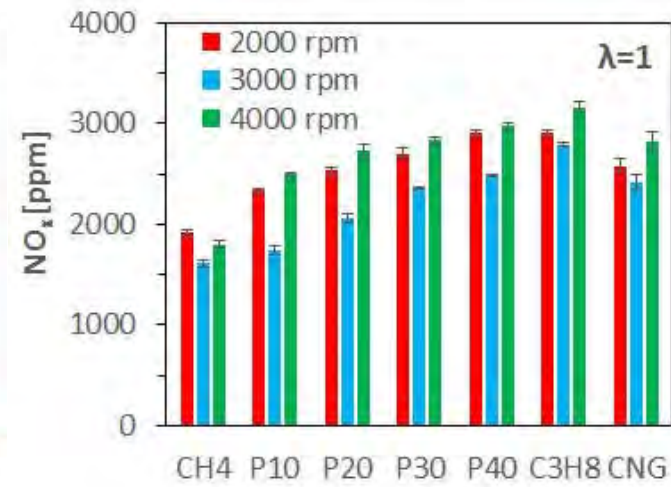
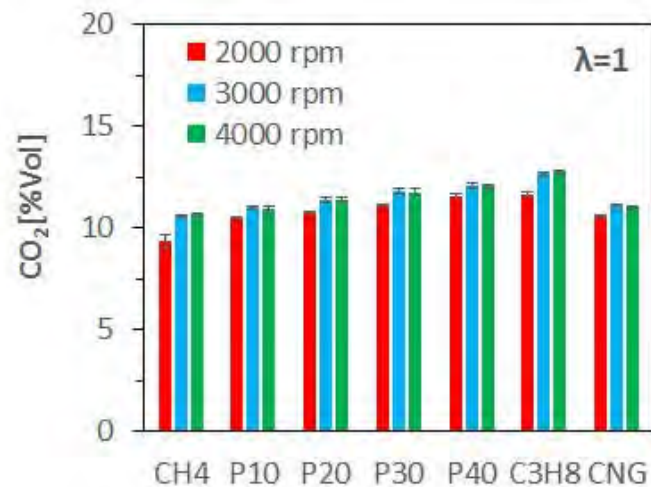
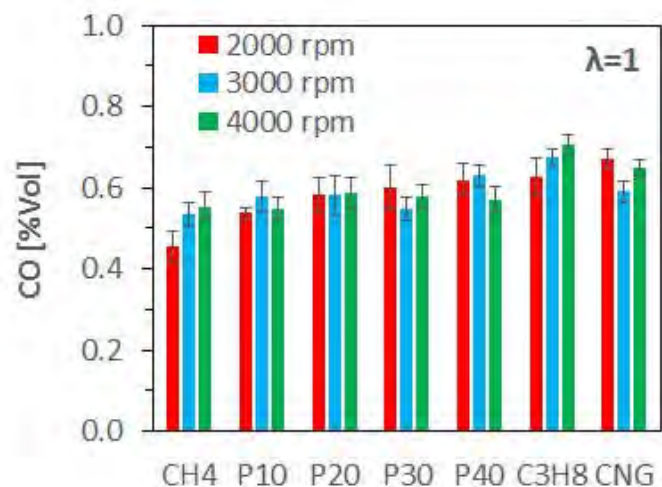
3 Miscele gassose real-time

Idee sul monitoraggio e il controllo della combustione



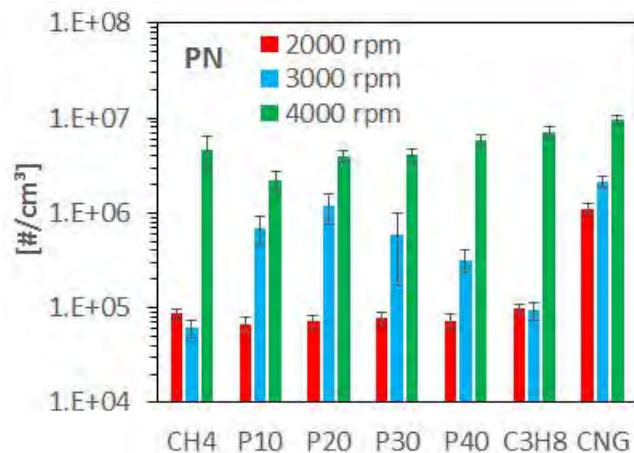
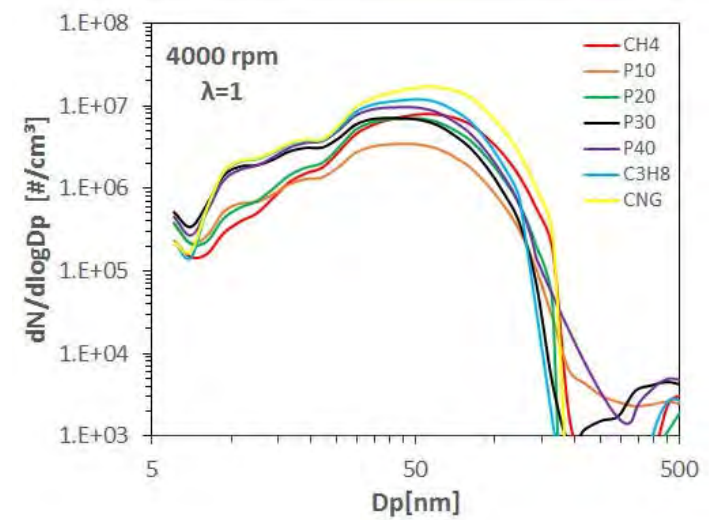
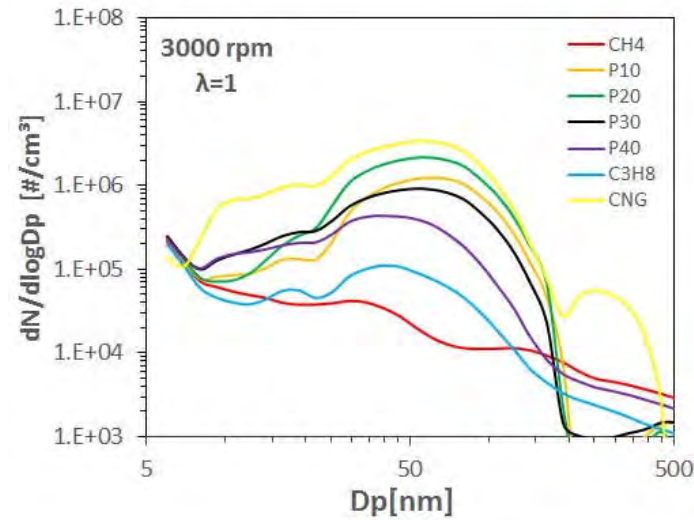
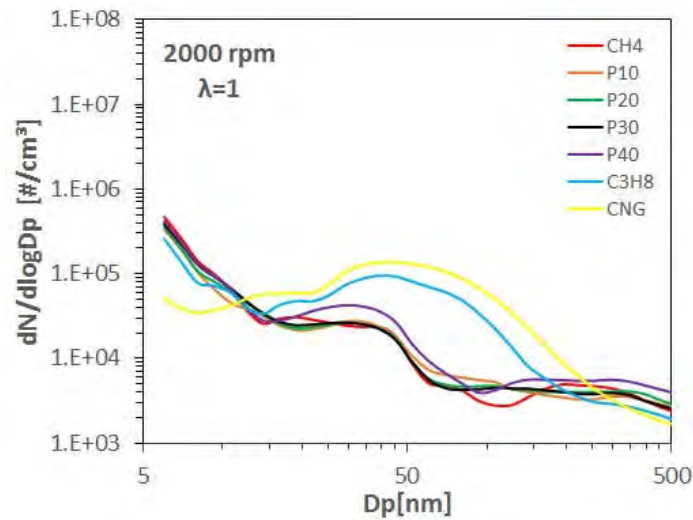
3 Miscele gassose real-time

Idee sul monitoraggio e il controllo della combustione



3 Miscele gassose real-time

Idee sul monitoraggio e il controllo della combustione

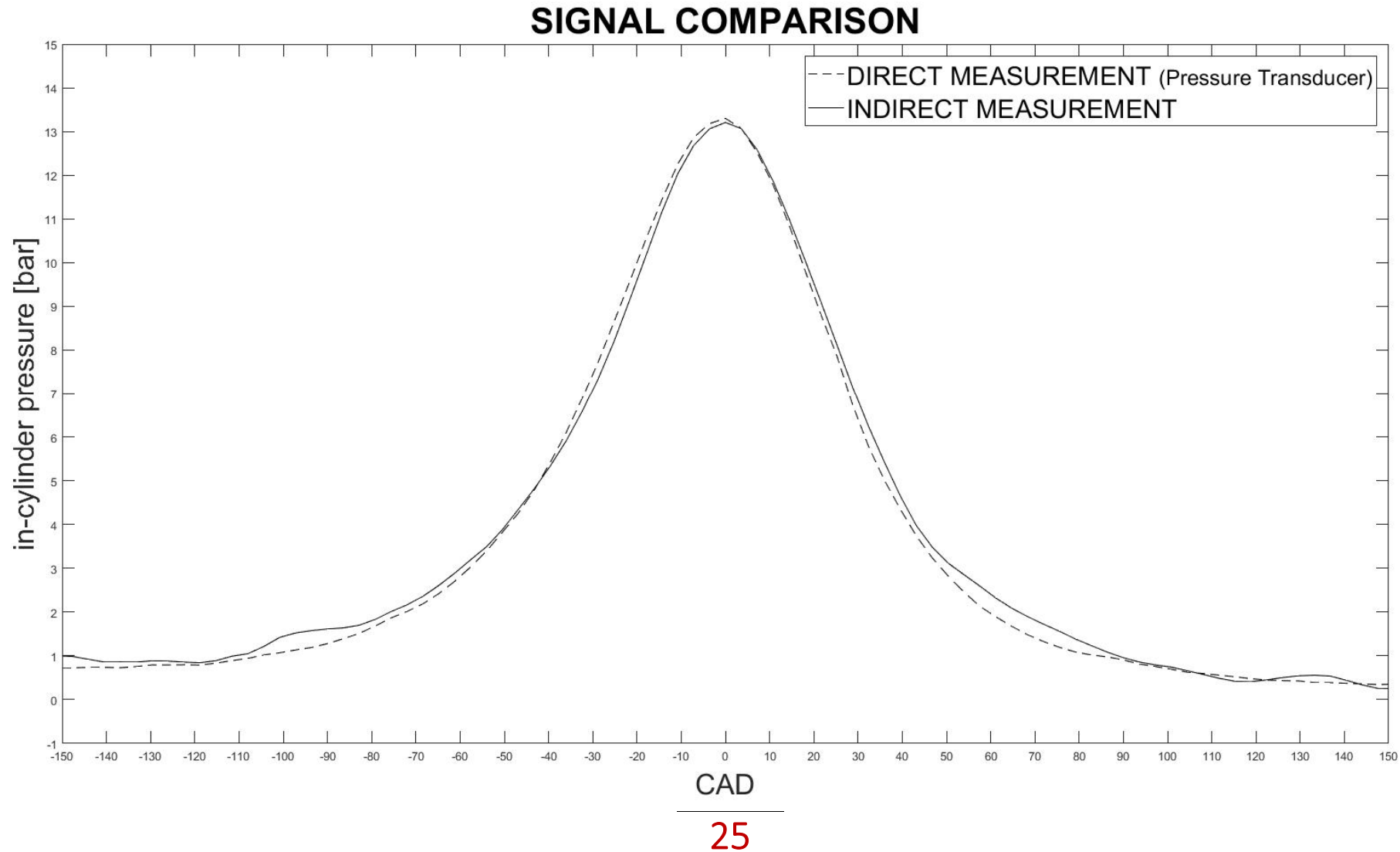


Amirante R, Distaso E, Di Iorio S, Sementa P, Tamburrano P, Vaglieco B.M., Reitz R.D.
Effects of Natural Gas Composition on Performance and Regulated, Greenhouse Gas and Particulate Emissions in Spark-Ignition Engines. Energy Convers Manag 2017;143:338–47.
 doi:10.1016/j.enconman.2017.04.016

Amirante, R., Distaso, E., Di Iorio, S., Pettinicchio, D., Sementa, P., Tamburrano, P., Vaglieco, B.M.
Experimental Investigations on the Sources of Particulate Emission within a Natural Gas Spark-Ignition Engine. SAE Technical Paper 2017-24-0141. doi:10.4271/2017-24-0141

3 Misura a basso costo della pressione in camera

Idee sul monitoraggio e il controllo della combustione



Grazie per l'attenzione

Elia Distaso

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