



Control Oriented Modeling of Internal Combustion Engines

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eProLab overview

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Augusto Tortora, Ph.D. Student

Main current partners...



■ 50% - EU
■ 35% - Private
■ 15% - Public

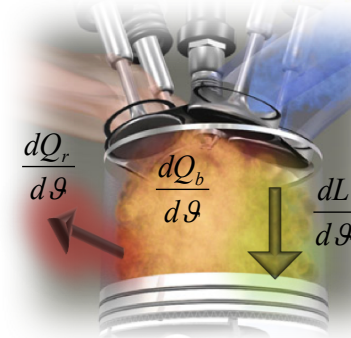
Research fields

Working Areas

- Engines, hybrid powertrains
- Non-conventional energy technologies (Fuel Cells)
- Simulation models for control, diagnosis, design and optimization

ICE Modeling & Control

- CI/SI combustion/emissions
- Vehicle / powertrain
- After-treatment system
- Emissions' virtual sensors
- Pressure based control/diagnosis



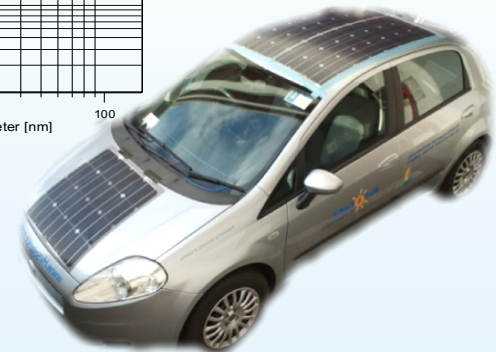
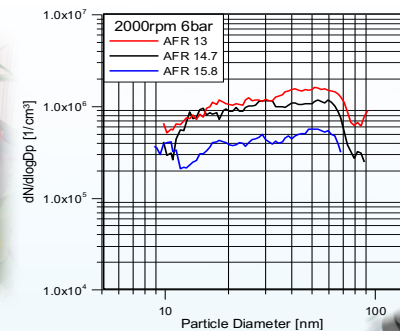
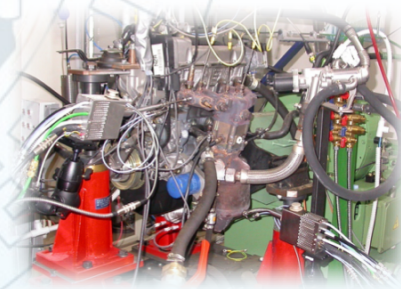
Adapted from <http://ralph-dte.eu>

Eco-Innovation Technologies

- Hybrid and hybrid solar vehicles
- WHR technologies (TEG, E-turbo, ORC)
- ADAS / Electronic Horizon

Facilities

- Fully equipped engine test bench
- Indicating equipment
- Emissions analyzers (HC, CO_x, NO_x)
- Combustion fast NO_x analyzer
- Smoke meter
- SMPS system for nano-particulate
- dSpace MicroAutobox & Etas INCA
- Two solar hybrid vehicle prototypes
- Two Fuel-Cells test benches



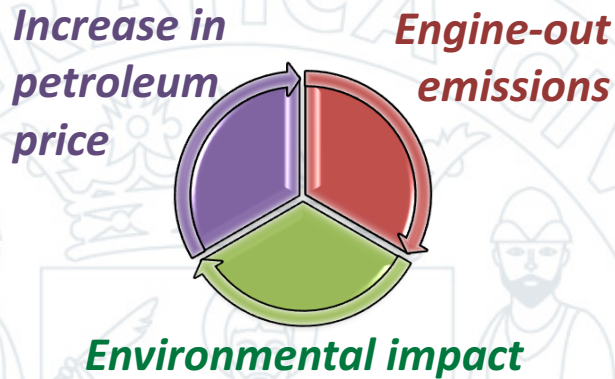
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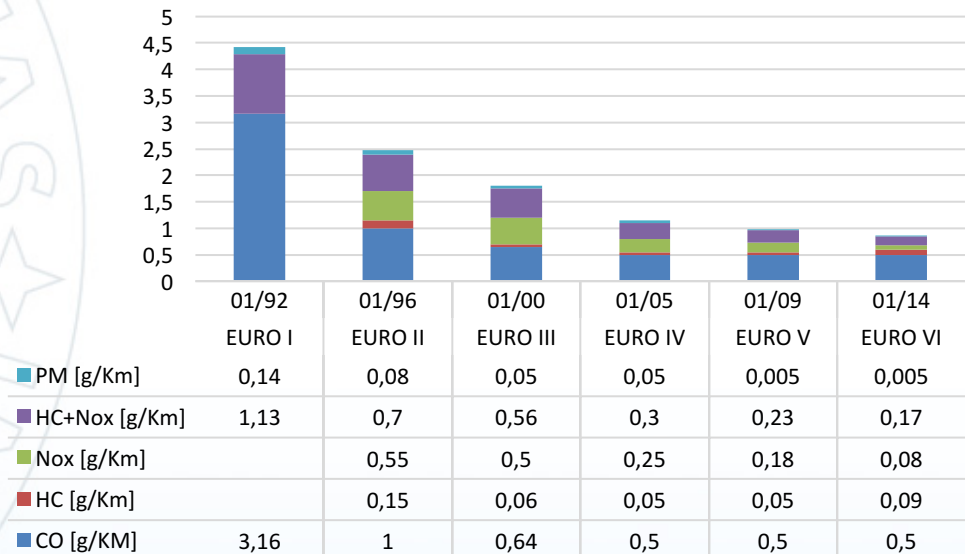
Modeling of SCR for Control Application

**Enhancement of fuel economy by ADAS and
Electronic Horizon**

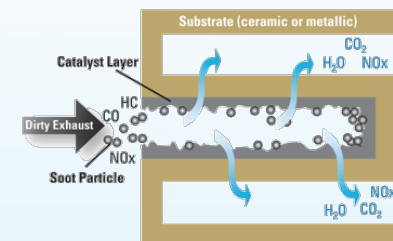
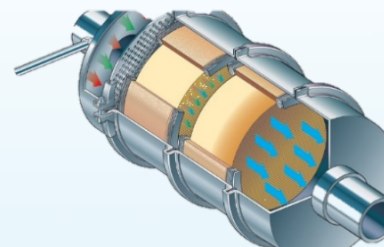
Context & motivations



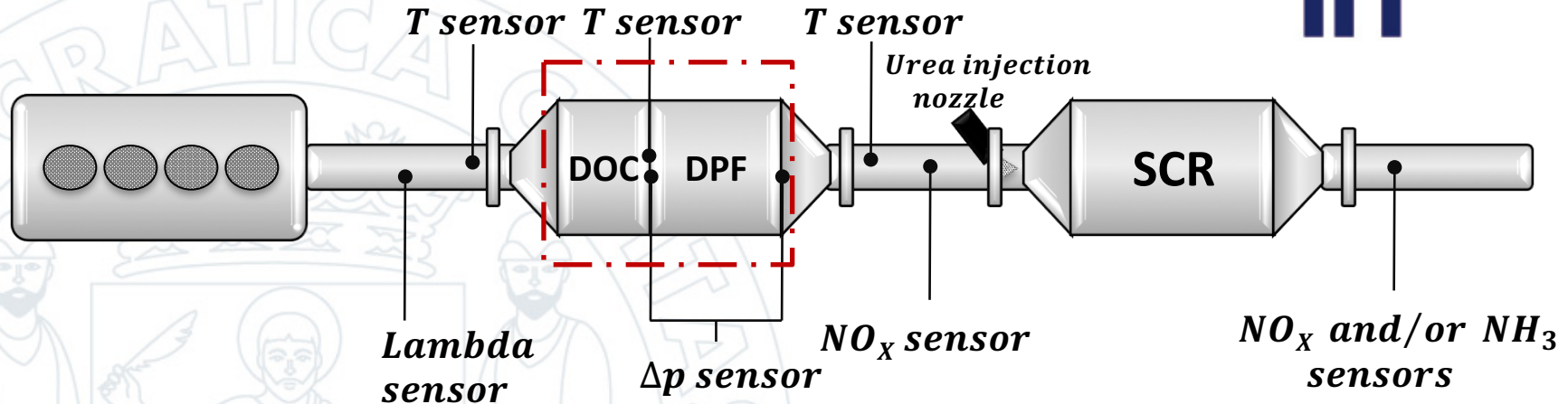
In order to comply with *emission targets* and *RDE test procedure* an optimized integration between combustion process and exhaust AT systems is mandatory.



With current technologies, the most suitable after-treatment devices for the abatement of NO_x and PM emissions are the **SCR and DPF systems**.



ATs layout



DOC – Diesel Oxidation Catalyst

- Oxidation of HC and CO
- Oxidation of NO to NO_2

✓ Accumulation

✓ Depth filtration

The particles fill the pores - High filter losses and moderate collection efficiency.

✓ Cake deposition

Soot layer builds up on the channel surface - Linear increase in pressure drop and high filtration efficiency.

DPF – Diesel Particulate Filter

✓ Regeneration

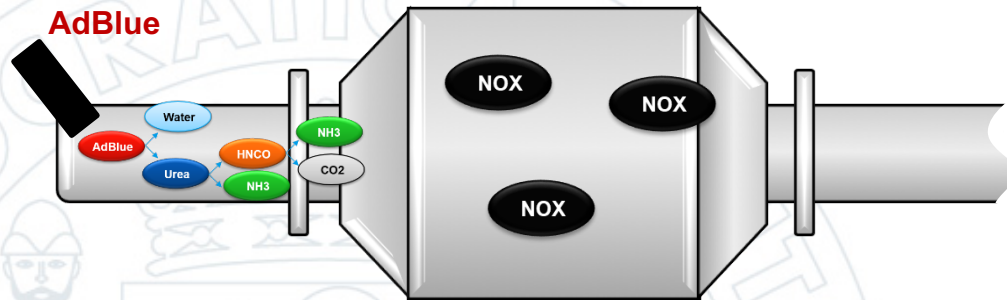
✓ Active

Enabled by an increase of gas temperature (suitable injection strategy / external source)

✓ Passive

Promoted at lower temperature by NO_2

SCR - main chemical phenomena

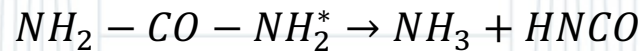


To supply the reducing agent (NH_3) required for SCR operation, a 32.5% aqueous urea solution (DEF - AdBlue) is injected for toxicity reasons.

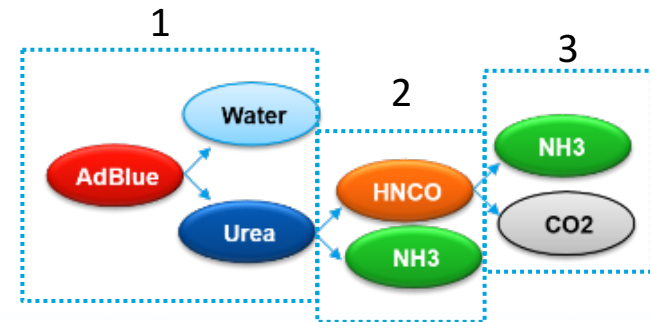
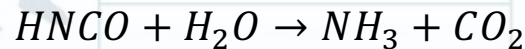
1. Urea **evaporation**



2. Urea **decomposition**



3. Isocyanic acid (HNCO) **hydrolyzation**

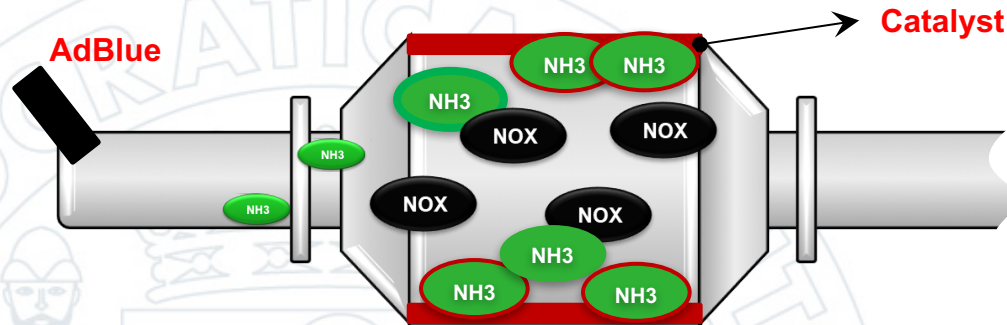


- **Catalyst;**
- High exhaust **temperature;**
- Optimal design of dosing unit.



Ideally, 100% urea to ammonia conversion can be expected at the very beginning part of the SCR catalyst.

SCR - main chemical phenomena



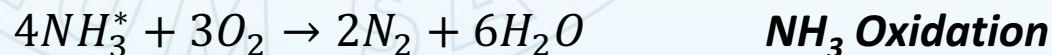
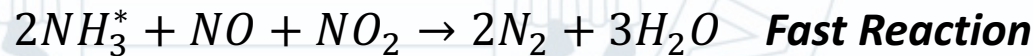
The key parameter in ammonia dynamics is the **total NH_3 adsorption capacity** Ω that is strongly dependent on temperature.

Adsorption & Desorption



Adsorbed NH_3 in the free active sites S_{free}

de NO_x reactions



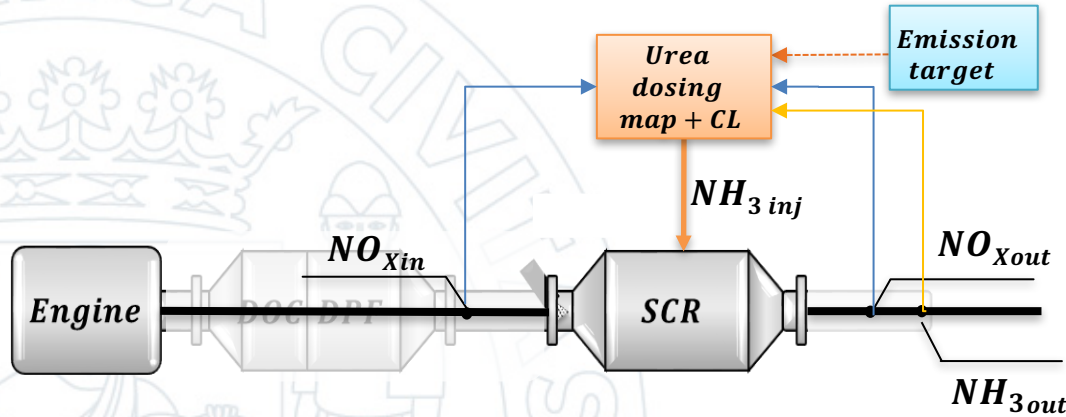
Negligible at Low Temperature

The **kinetic rates** are strictly related to the free catalytic sites available on the catalytic substrate

SCR map based control



Objective: optimization of Urea dosing strategies to reach balance between high NO_x reduction efficiency and low NH_3 slip



Non linearities of the system

- Reaction kinetics
- Cross sensitivity of NO_x sensor to NH_3

System dynamics

- Catalyst Temperature
- Ammonia storage

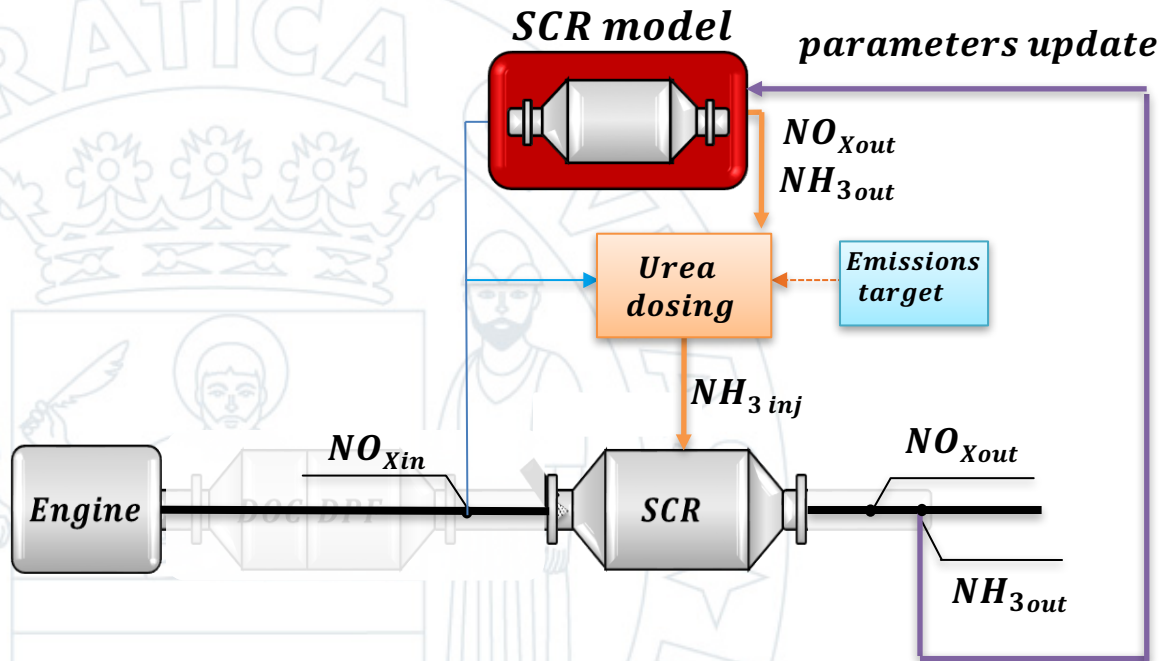
Transport delay

- From urea control signal to NH_3 in the catalyst

Uncertainties

- Engine out gas temperature, flow and composition (i.e. NO , NO_2);
- Thermal state of the SCR;
- NH_3 injection accuracy, deposits.
- Sensor accuracy
- SCR actual NH_3 storage, formulation, aging

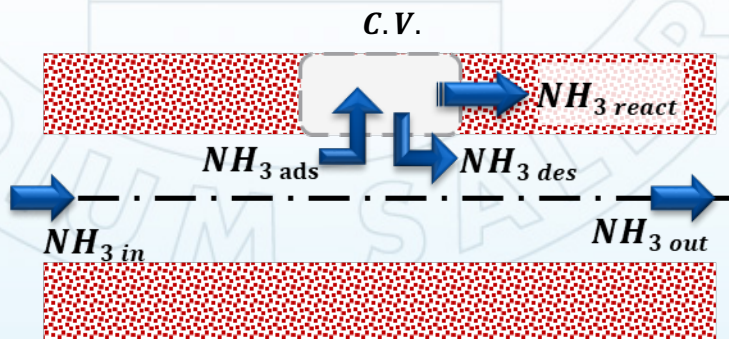
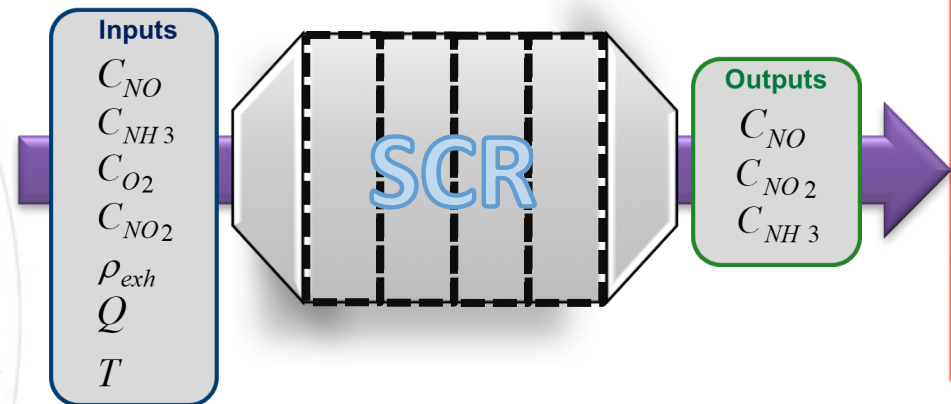
SCR model based control



- Prevent ammonia slip during transients;
- Optimize NO_x conversion efficiency by maximizing NH_3 availability, especially during fast changing operation.
- Provide adaptive features vs. systems aging and plant-model mismatch by on-board **model parameters update**

SCR model formulation

- Lumped approach: SCR catalyst is partitioned into **4 section** along the axial direction;
- Mass balance of chemical species involved;
- Mass transport neglected, **chemical kinetics** in the catalyst are reaction controlled;
- Reaction rates are defined as a function of **ammonia storage (θ)** and gas phase concentrations of NO and NO₂ by Arrhenius like formulation.



The interaction of ammonia with catalytic substrate is represented by **ammonia coverage ratio (θ)**

$$\vartheta = \frac{C_{NH_3}^*}{\Omega}$$

SCR model equations

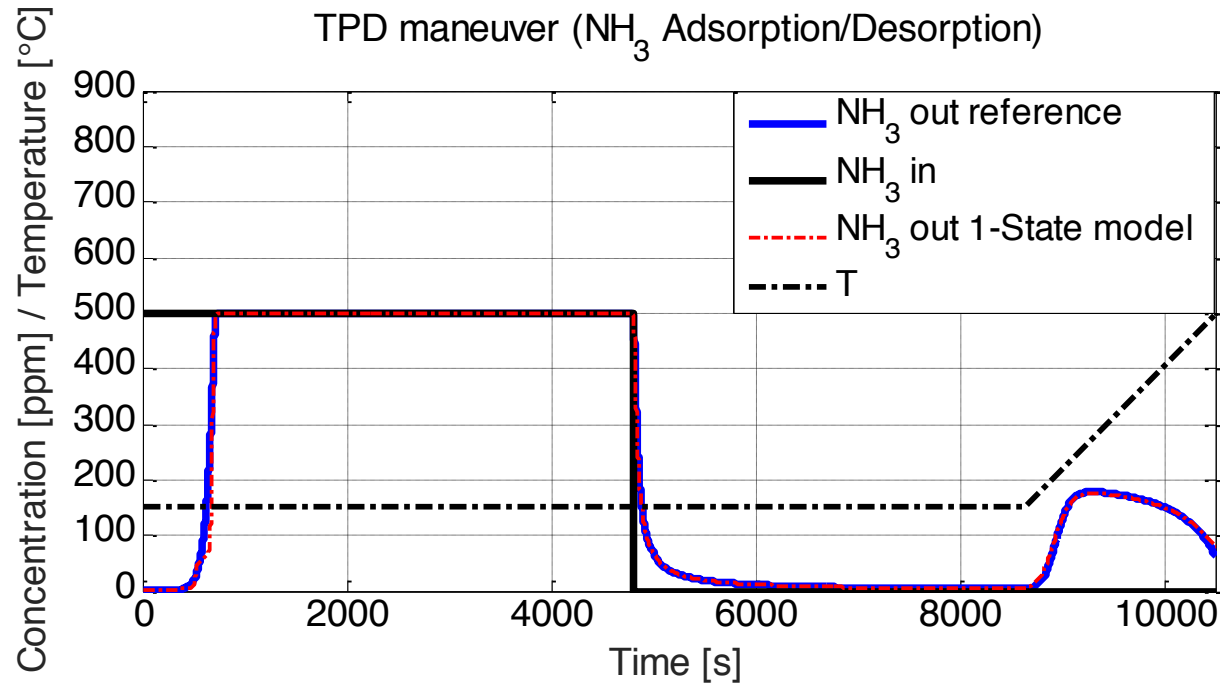
$$\begin{bmatrix} 0 \\ 0 \\ \dot{\vartheta} \\ 0 \end{bmatrix} = \begin{bmatrix} -\bar{Q}C_{NO} - K_{fast}\vartheta\Omega C_{NO}C_{NO_2} - K_{std}\vartheta\Omega C_{NO}C_{O_2} + \bar{Q}C_{NO_{in}} \\ -\bar{Q}C_{NO_2} - K_{fast}\vartheta\Omega C_{NO}C_{NO_2} - K_{slow}\vartheta\Omega C_{NO_2} + \bar{Q}C_{NO_{2in}} \\ -(K_{des}+K_{oxi})\vartheta + K_{ads}C_{NH_3}(1-\vartheta) - K_{fast}\vartheta C_{NO}C_{NO_2} - K_{std}\vartheta C_{NO}C_{O_2} - K_{slow}\vartheta C_{NO_2} \\ K_{des}\Omega\vartheta - [K_{ads}\Omega(1-\vartheta) + Q]C_{NH_3} + \bar{Q}C_{NH_{3in}} \end{bmatrix}$$

- The computational burden is not suitable for on-board control application.
- NO, NO₂ and NH₃ concentration dynamics are much faster than the ammonia storage.
- Reduction to one-state model with ϑ as only dynamic process to be modelled.

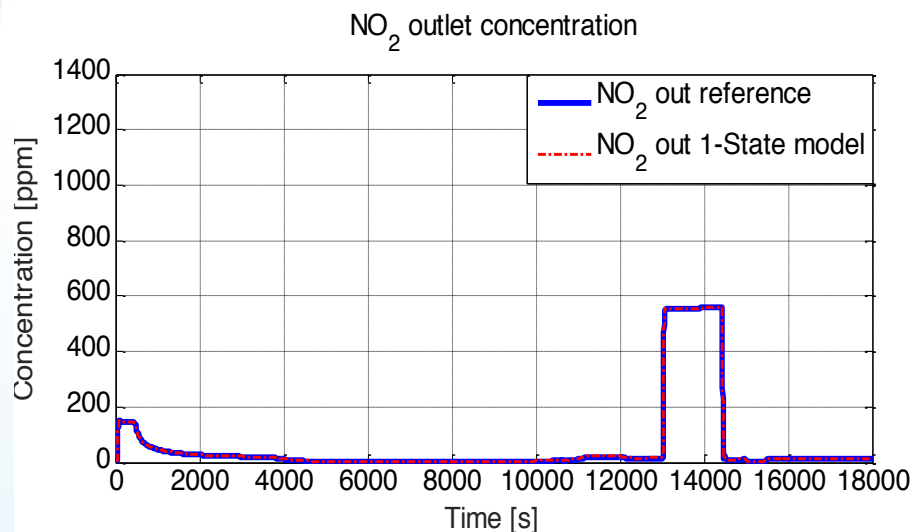
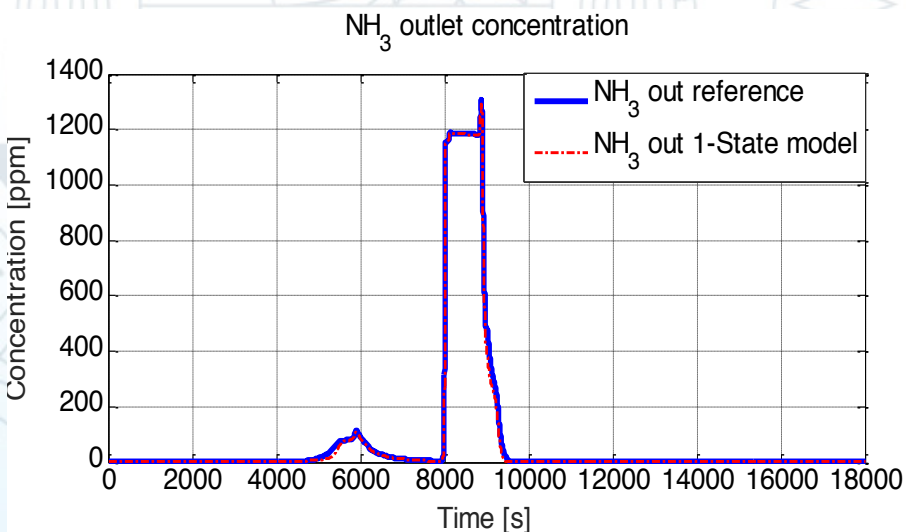
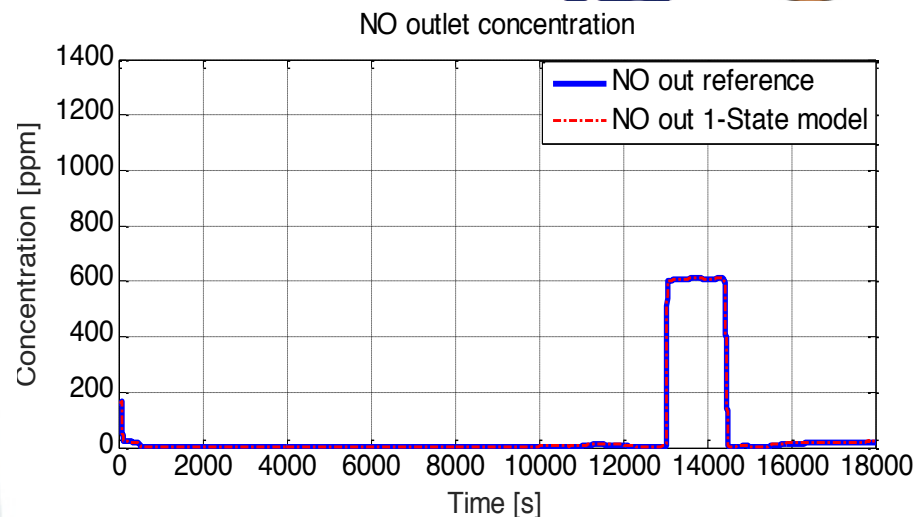
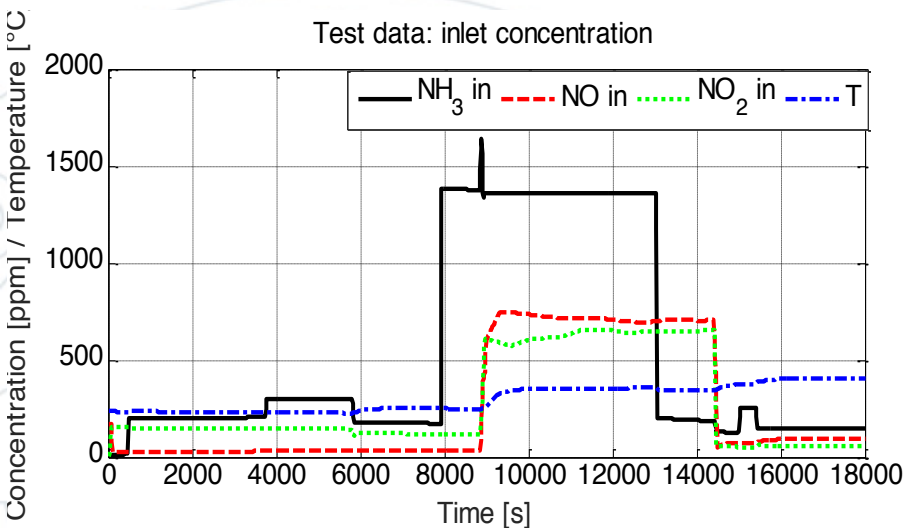
SCR model parameters identification



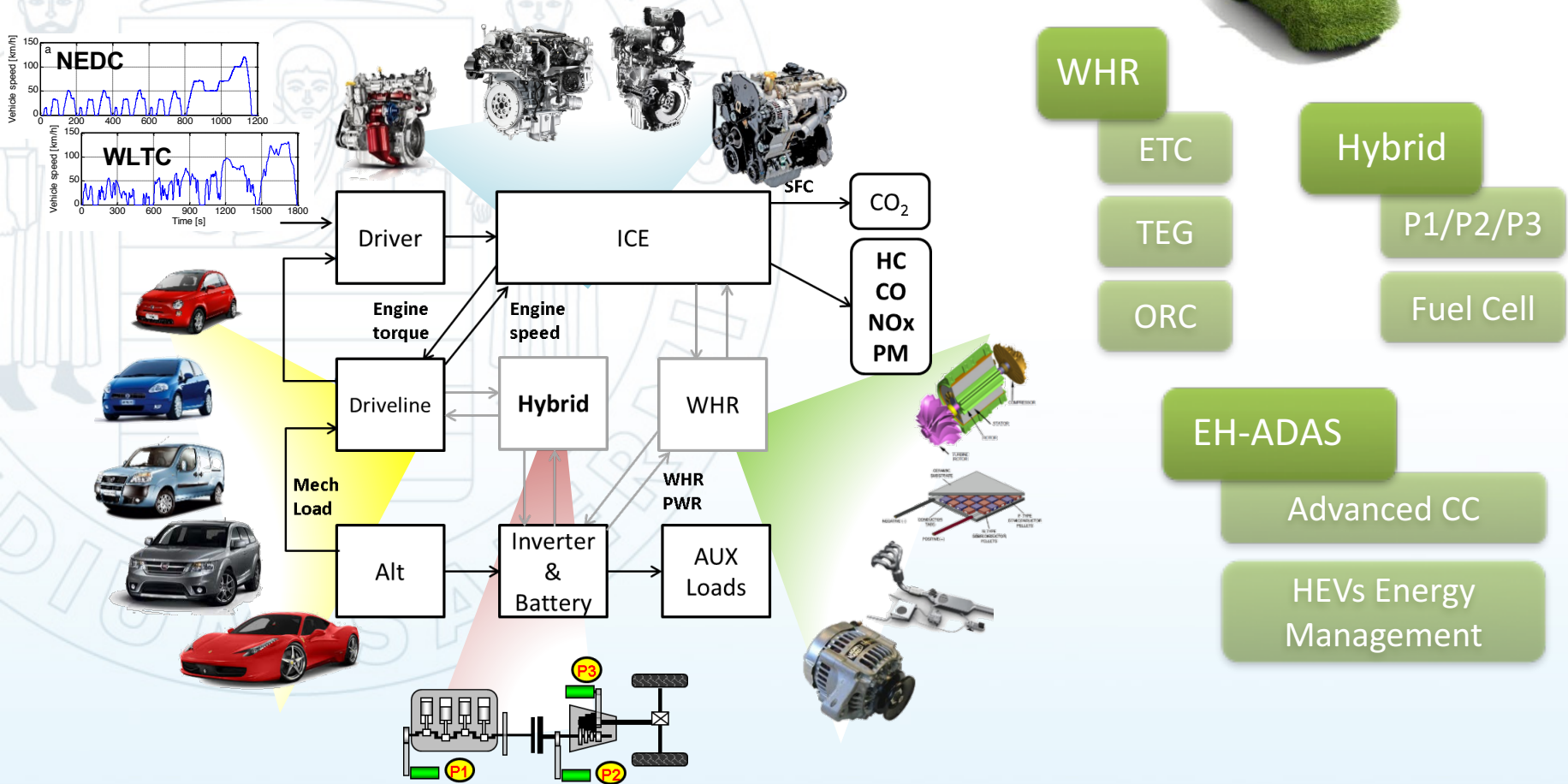
Temperature Programmed Reaction at the Hot Flow Bench



SCR model validation - TPR tests



diin Dipartimento di
Ingegneria Industriale



From EH to Engine

Mission domain

Powertrain domain



Deterministic variables

OPTIMIZATION

EH
ADAS

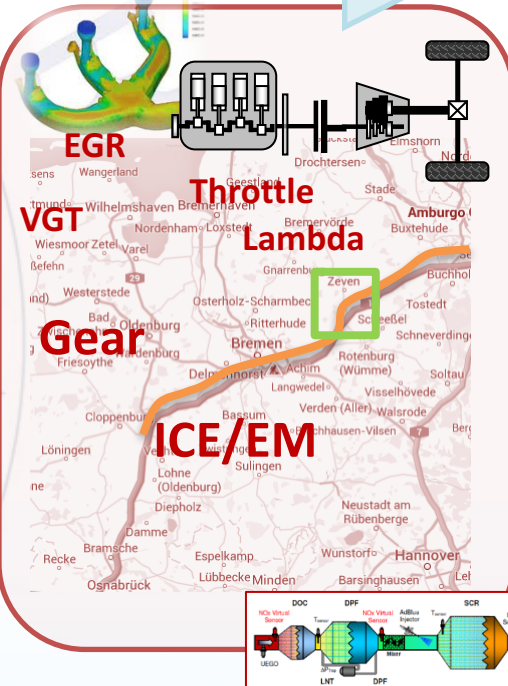


Speed

V2X



Stochastic variables



FEEDBACK

Max fuel economy with constraints on

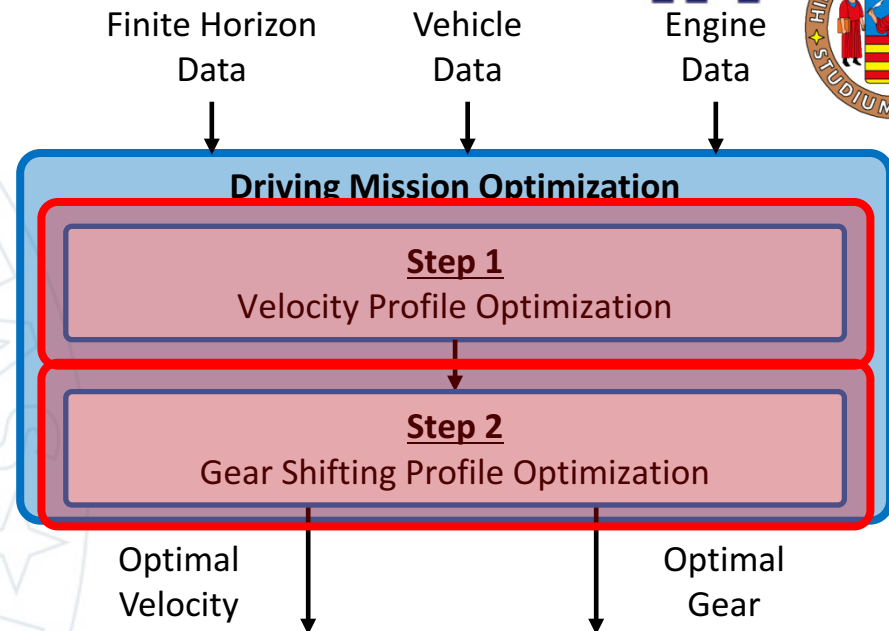
V_{avg} , V_{max}
NOx, PM
SOC

Proposed Approach



The proposed approach splits the optimization problem:

1. compute a velocity profile that minimizes the energy spent to move the vehicle along the route;
2. choose the gear or the ICE/EM torque demand entailing the minimum fuel consumed to follow the velocity reference computed in the first step.



Step 1

$$J_k(\bar{u}_k, \bar{x}_k) = J_k(u_F, K_k) = \Delta x \left(F_{drv,k}^2 + \mu \max \left(0, (v_{avg} - v_k) \right) \right)$$

Step 2

$$J_k(\bar{u}_k, \bar{x}_k) = J_k(u_{sh,k}, \gamma_k) = \frac{\dot{m}_{f,k} v_k}{\Delta x} + \Phi K_{loss,k} u_{sh,k}$$

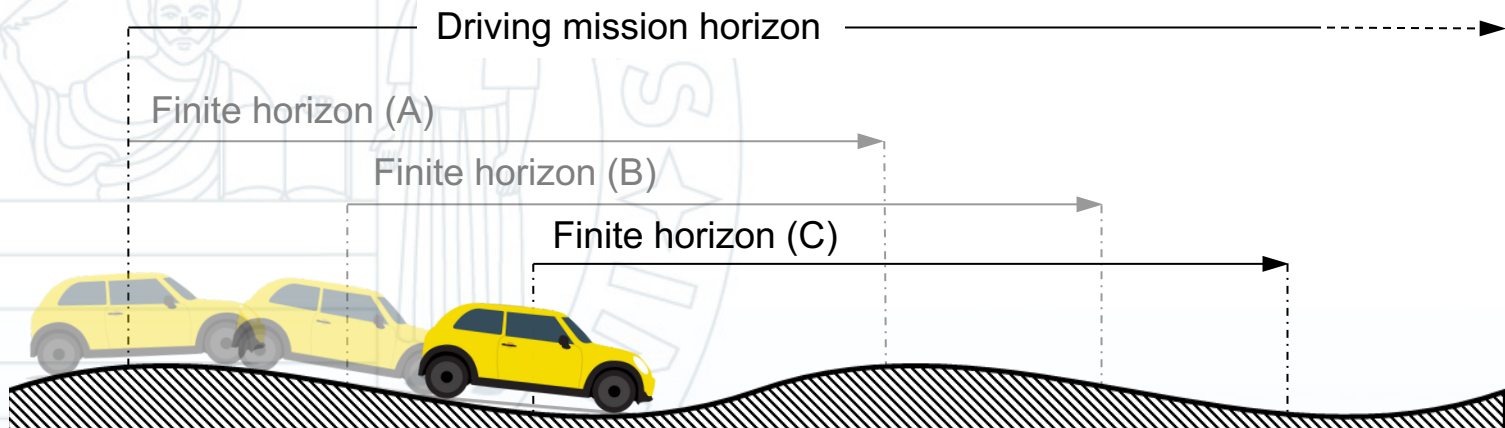
Rolling Horizon Approach

Real driving scenarios are characterized by

- **traffic flows**
- interactions with **surrounding vehicles**
- **traffic lights...**

which can prevent the calculated optimal velocity from being tracked.

The optimal control problem is solved for a **finite rolling horizon**.



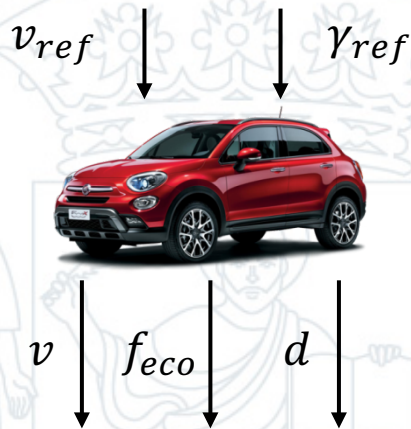
- Sub-optimality of the solution
- Updates the optimal control law each 500 m
- Reduces the calculation time and memory usage (that are fixed)
- Dynamic adaptability to the environmental changes
- ... optimization can be triggered if the vehicle drifts from the optimal reference



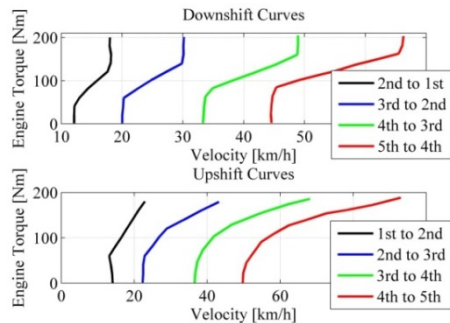
Approaches Comparison



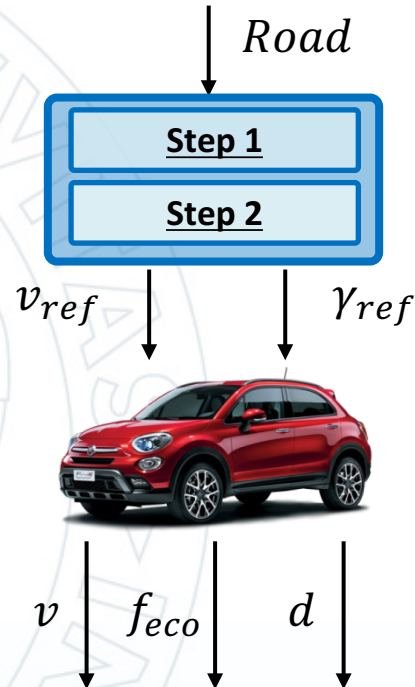
Classic Cruise Controller - CC



Fixed velocity set-point and shifting maps

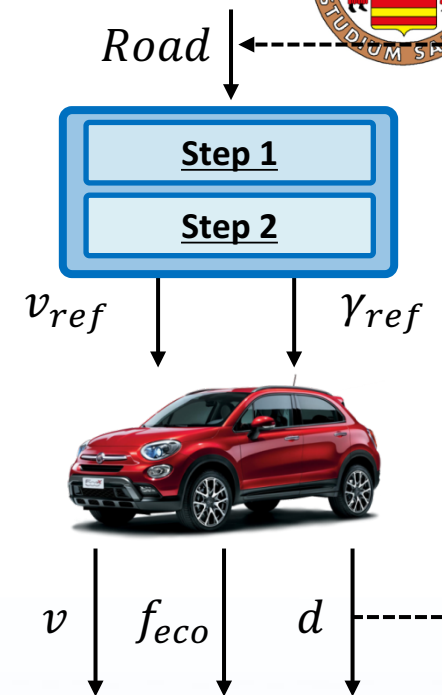


Entire Horizon - EH



DP Optimization over the entire mission horizon

Finite Horizon - FH



DP Optimized over a finite rolling horizon approach

Driving mission horizon

Driving mission horizon

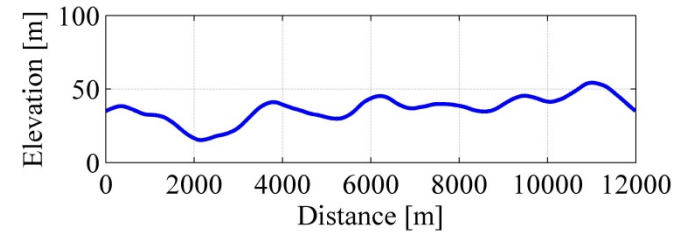
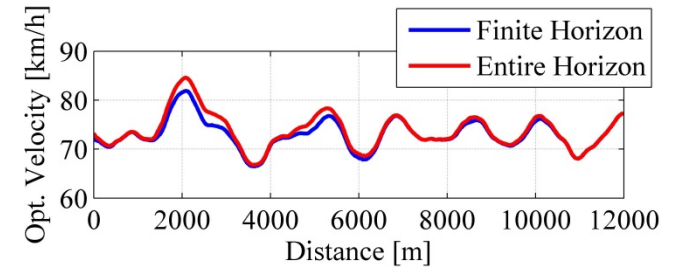
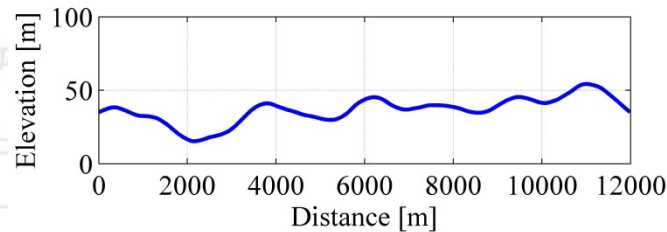
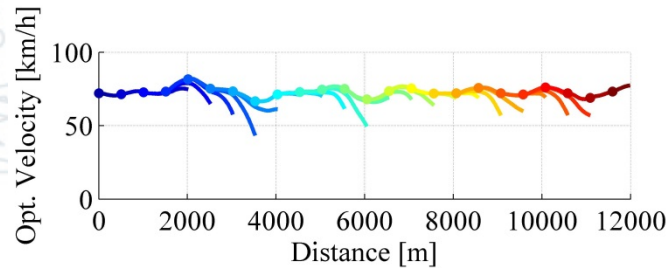
Finite horizon (A)
Finite horizon (B)
Finite horizon (C)



Simulation Results

Scenario #1

- Three-lanes highway
- 12 km
- $\alpha \in [-2.7\%, +3.1\%]$
- $v_{max} = 90 \text{ km/h}$



	Time [s]	$\Delta time$ [%]	Fuel Eco [km/l]	$\Delta fuel$ [%]
CC	584.8	-	26.82	-
FH	579.3	-0.94	27.85	-3.84
EH	575.1	-1.66	28.12	-4.85



Thank You

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